

HALF BAND FILTERS FOR MULTISTAGE INTERPOLATOR

Nisha Chakrawarti¹, Prof. Sachin Singh²

^{1,2} Department of Electronics & Comm. Engineering,
Shri Ram Institute of Science & Technology,
Jabalpur, (M.P.)

Abstract – In single-stage filters are proficient for the lower request interpolation factors, yet for the high rate change (which is needed in the advanced computerized correspondence frameworks like WCDMA), the single-stage execution doesn't give adequately powerful reaction. Accordingly for these applications under comparative conditions, the multi-stage execution of the interpolator might be liked. Further, the effective execution of advanced introduction frameworks for the up-examining of QAM (quadrature amplitude modulation) /QPSK(quadrature phase shift keying) based multi-stage computerized interpolators have likewise been proposed. Here, the complete yield power improves from - 25.19 dBm to - 22.96 dBm, and the top to average force improves from 6.166 dB to 6.106 dB in the QAM based twofold stage interpolation filter. The all out yield power improves from - 28.09 dBm to - 25.84 dBm, and the top to average force improves from 3.181 dB to 3.158 dB in the QPSK based twofold stage interpolation filter. Yet, the multi-stage execution thus builds the computational just as execution intricacy of the general correspondence framework

Key Words:QAM, QPSK, WCDMA , Multisatge filter and interpolator

1.INTRODUCTION

Multi-rate signal allotment procedures are broadly utilized in a few spaces of contemporary designing like interpolation factors, picture handling, advanced sound, and media. The significant advantage of a Multi-rate framework is the extensive lessening of computational thickness, and thusly, the substandard force use continuously activities, slighter chip region seek after by the expense decrease. The computational skill of Multi-rate calculations is platform on the capacity to

utilize simultaneously different model rates in the unique pieces of the plan. Also, the Multi-rate-based calculations are worn to settle a couple of the composite sign handling tasks that couldn't be resolve in any case, for example, representation rate transformations, signal crumbling and remaking, multiplexing and de-multiplexing, adding up to of DSP changes. Multi-rate frameworks are structure impedes every now and again utilized in computerized signal handling their motivation is to change the beat of the discrete-time signals, which is acknowledge by adding or delete a piece of the sign delineation.

2. MULTI-STAGE IMPLEMENTATION OF AN INTERPOLATOR

The above discussed structures are the single stage filters which are suitable interpolation of lower order. This couldn't be used for higher orders. For these domains a multi-stage [14, 29] interpolator is suggested. The interpolation factor L is factorized into multiplication of integers like, $L = L_1 L_2 \dots L_K$ and applied as K cascade interpolators as in figure

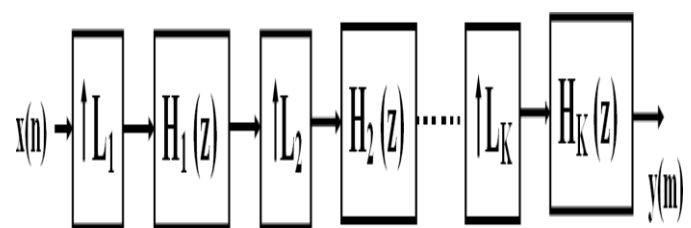


Figure 1: Multi-stage interpolator

The immediate structure just as the poly-stage constructions can be utilized proficiently utilizing the multi-stage execution, which prompts less computational intricacy in the execution of an interpolator [15]. The multi-stage execution of an interpolator brings about the decrease of computational intricacy, less capacity necessity in the framework, and they worked on channel plan. In spite of these benefits, the multi-stage execution has following deficiencies

- The number of phases of the framework cannot be expanded past a specific worth in light of the fact many that period, the intricacy of the framework begins expanding.
- Appropriate control structure is needed to deal with every one of the phases of the basic framework

3. LTH BAND LINEAR PHASE FILTERS

The digital Lth band filters are the specified category of digital filters, which works for both single and multi rate signal processing. Cut-off angular frequency is located at π/L for Lth band low pass filter and transition band is distributed around this frequency. In time-domain, the impulse response of an Lth band digital filter has zero valued samples at the multiples of L samples counted away from the central sample to the right and left directions. In reality, an Lth band filter has zero crossings at the regular distance of L samples, thus fulfilling the well known zero inter-symbol interference Property.

4. Proposed Work

The decimators and interpolators talked about so far are single-stage frameworks since the execution plans comprise of a solitary low-pass channel and single examining rate adjustment gadget. At the point when the decimation factor M can be figured into the result of whole numbers, $M = M_1 \times M_2 \times \dots \times M_K$, rather than utilizing a solitary channel and factor-of - M down-sampler the by and large decimator can be carried out as a course of K decimators. Such a course execution, called a multistage decimator.

In a similar way, the factor-of-L interpolator expressible by $L = L_1 \times L_2 \times \dots \times L_K$, can be carried out as a course of K interpolators as portrayed in Figure. The course execution plan of Figure is known as the multistage interpolator. The multistage structure from Figure replaces the single stage decimator of the factor $M = M_1 \times M_2 \times \dots$

M_K . The transfer function $H(z)$ of the same single-stage pulverization channel can be acquired by applying the third personality to the execution plan of Figure. The course of K decimators of Figure gives the accompanying comparable transfer function $H(z)$,

$$H(z) = H_1(z) H_2(z^{M_1}) H_3(z^{M_1 M_2}) \dots H_K(z^{M_1 M_2 \dots M_{K-1}})$$

Accordingly, the single-stage structure demonstrated in Figure is comparable to the construction. Additionally, the general exchange work for the K stage interpolator is gotten while applying the 6th personality to the multistage execution construction of Figure. Along these lines, we get,

$$H(z) = H_1(z) H_2(z^{L_1}) H_3(z^{L_1 L_2}) \dots H_K(z^{L_1 L_2 \dots L_{K-1}})$$

The relating single-stage equality for the K stage interpolator is shown in Figure. The multistage structures are extremely helpful for executing enormous inspecting rate change factors. A solitary obliteration/introduction channel with an exceptionally restricted pass band, typically awkward for the plan and execution, is supplanted with the course of easier channels. The details for those singular channels are fundamentally loose since the general channel particular is divided among a few lower-request channels. We show the impacts of the multistage execution in MATLAB on the case of a three-stage decimator with the factor $M = 8$. Since the mentioned factor M is the force of two, $M = 8 = 2^3$, we utilize the indistinguishable channels in the course of Figure. Thus, we plan just one channel and utilize this channel in every one of three decimator stages.

4.1 HALF BAND FIR FILTERS

A half band filter is a Lth-band filter with $L = 2$, and therefore, the half band filter partitions the baseband of the sign into two equivalent subbands. In the direct stage half band filter, a big part of the constants are zero-esteemed making the execution exceptionally appealing.

4.2 LINEAR-PHASE HALF BAND FILTERS

The transfer function of a linear-phase FIR half band filter is given in the form

$$H(z) = \sum_{n=0}^{2K} h[n]z^{-n}$$

Where, K is odd, and coefficients are symmetric in respect to the central coefficient $h[K]$,

$$h[2K - n] = h[n], \text{ for } n = 0, 1, \dots, 2K.$$

The filter length N is an odd number

$$N = 2K + 1, K = 1, 3, 5, \dots$$

The time-domain conditions defined by equation for an L th-band filter, in the case of a half band filter become

$$h[K] = 1/2, h[k+2r] = 0 \text{ for } r=1, 2, \dots, [K/2]$$

This equation says that the odd-indexed coefficients in $\{h[n]\}$ are zero-valued except for the central coefficient $h[K]$, which is equal to $1/2$. Since K is an odd number, the impulse response begins and terminates with nonzero samples, $h[0] \neq 0, h[2K] \neq 0$. Figure illustrates the impulse response of a typical linear-phase FIR half band filter. The impulse response shown in Figure 7.7 has the length of $N = 11$ samples, giving $K = (N-1)/2 = 5$. Since K should be odd, the filter length can be augmented (diminished) by the multiple of four samples. Hence, we can choose $N = 7, 11, 15, 19, \dots$. In the frequency domain, the zero-phase frequency response of a half band filter exhibits symmetry property.

$$H(w) + H(\pi-w) = 1$$

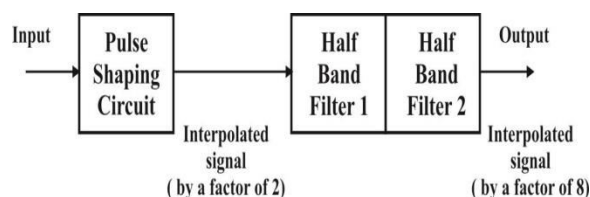


Figure 2: Three-stage interpolator using half-band filter

5. RESULTS AND DISCUSSION

Extra plan effectiveness can be accomplished by utilizing a few fell multirate stages, which lessens the absolute number of channel coefficients. For instance, rather than carrying out a plan dependent on a solitary destruction factor of 48, we could consider two phases of annihilation utilizing 12 and 4, or 24 and 2, or some other blend of elements that increase to 48.

For executing, the three-stage interpolator without utilizing the half-band channel, we have associated three interpolators in the course which comprises of two DUC channels (each channel added by 2) trailed by the beat forming circuit (inserted by 2) with the accompanying determinations

- Sampling Frequency: 46.08MHz
- Bandwidth: 5 MHz
- Interpolation factor: 8

To execute, the three-stage interpolator utilizing the half-band channel, we have associated three interpolators in course, which comprises of the beat molding circuits (interjected by 2) trailed by the two half-band channels (every half band channel added by 2) with the accompanying details

- Sampling Frequency = 46.08MHz
- Bandwidth = 5 MHz
- Interpolation factor = 8

The output spectrum of three-stage interpolator with the half-band filter is shown in figure.

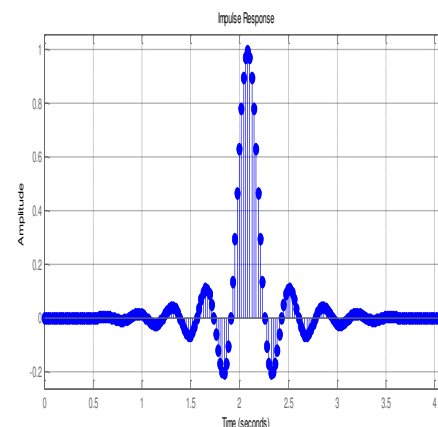


Figure 3: Impulse response of filter

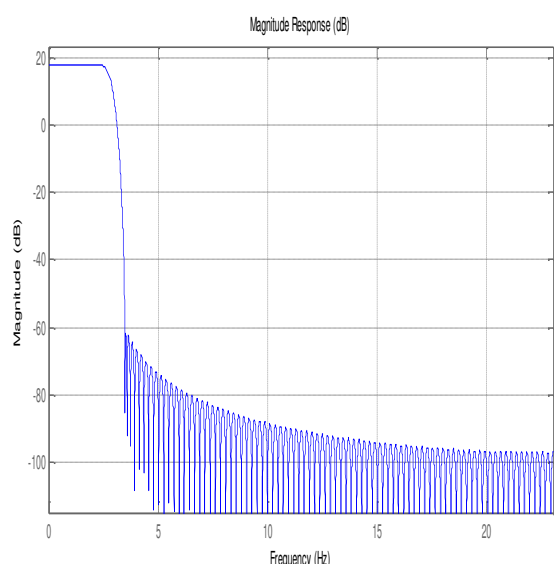


Figure 4 : Magnitude response of filter

The reproduction results show that the execution of single-stage interpolator prompts the stop-band edge recurrence of 14.6 MHz; however for the three-stage interpolator, this stop-band edge decreases to 6.7 MHz with more keen recurrence reaction in the stop-band area. Thusly, the introduced three-stage interjection gives similarly a more keen progress comparative with the single-stage addition. Further, the stop-band edge recurrence diminishes to 3.7 MHz because of the utilization of half-band channels for the three-stage interpolators. Furthermore, the decrease in the quantity of multipliers utilizing the multi-stage interpolators has been displayed in the table

Table 1: Comparison of Interpolator

Bandwidth (MHz)	Single-stage interpolator (multipliers)	Three-stage interpolator (multipliers)	
		Without half- band filters	With half-band Filters
20	59	55	50
15	117	82	71
10	229	109	80
7.5	462	128	102
5	384	112	82

The table demonstrates the quantity of channel taps just as the multipliers required and furthermore the decrease in the quantity of multipliers for the three-stage interpolator utilizing the half-band channel. This table additionally diagrams that the quantity of multipliers fundamental for the three-stage interpolator utilizing the half-band channels is not exactly that of the quantity of multipliers essential for the single-stage interpolators and three-stage interpolator without utilizing the half-band channels. In contrast with the single-stage separating, the three-stage sifting (with and without half-band channels) with less number of multipliers (PSD) at the edge of channel data transfer capacity. Hence, it is apparent that the half-band channels are useful in planning the powerful and productive multi-stage computerized interpolators according to the execution perspective.

6. CONCLUSIONS

The essential imperative of advanced correspondence framework is the proficiency of the fundamental framework, which can be improved generally utilizing the multi-stage interpolators, as it is obvious from the yields. We can additionally work on the proficiency by falling increasingly more interpolators, however it ought to be remembered that the framework turns out to be increasingly more perplexing as the quantity of stages increments. This intricacy can be diminished radically by utilizing the half-band channels. The outcomes show that the quantity of multipliers fundamental for the three-stage interpolator utilizing the half-band channels is not exactly that the quantity of multipliers important for the single-stage interpolators and three-stage interpolator without utilizing the half-band channels. In any case, the general outcomes exhibit that the viability of the proposed conspire over the regular methodologies. The further improvement in the thesis can be accomplished by utilizing powerful hang pay channel stage.

REFERENCES

1. R. E. Crochiere and L. R. Rabiner, "Optimum FIR digital filter implementations for decimation, interpolation, and narrow-band filtering," *IEEE Trans. Acoust., Speech, Signal Process.*, vol. 23, no. 5, pp. 444-456, October 2020.
2. R.A. Meyer and C.S. Burrus, "Design and implementation of multirate digital filters," *IEEE Trans. Acous., Speech, Signal Process.*, vol. 24, no. 1, pp. 53-58, February 1979.
3. M. Vetterli, "A theory of multirate filter banks," *IEEE Trans. Acoust., Speech, Signal Process.*, vol. 35, no. 5, pp. 356- 372, March 1987.
4. P. Vaidyanathan, "Multirate digital filters, filter banks, polyphase networks, and applications: A tutorial," *Proc. IEEE*, vol. 78, no. 1, pp. 56-93, January 1990.
5. P. P. Vaidyanathan, *Multirate Systems and Filter Banks*. Englewood Cliffs, New Jersey: Prentice Hall, 2013.
6. E. B. Hogenauer, "An economical class of digital filters for decimation and interpolation," *IEEE Trans. Acoust., Speech, Signal Process.*, vol. 29, no. 2, pp. 155-162, April 1981.
7. T. Hentschel and G. Fettweis, "Sample rate conversion for software radio," *IEEE Commun. Mag.*, vol. 38, no. 8, pp. 142-150, August 2000.
8. A. A. W. Saud and G. Stuber, "Modified CIC filter for sample rate conversion in software radio systems," *IEEE Signal Process. Lett.*, vol. 10, no.5, pp. 152-154, May 2003.
9. A. K. Z. Jiang and A. N. Willson Jr., "Application of filter sharpening to cascaded integrator-comb decimation filters," *IEEE Trans. Signal Process.*, vol. 45, no. 2, pp. 457-467, February 1997.
10. G. Dolecek and S. Mitra, "A new two-stage sharpened comb decimator," *IEEE Trans. Circuits and Syst.-I*, vol. 52, no. 7, pp. 1414-1420, July 2005.
11. P. Savvopoulos and T. Antonakopoulos, "An IF digital down converter for software radio DVB-S2 receivers," in *Proc. 14th IEEE Int. Conf. Elect., Circuits, Syst.*, December 2007, pp. 1043-1046.
12. D. Babic, J. Vesma, and M. Renfors, "Decimation by irrational factor using CIC filter and linear interpolation," in *Proc. IEEE Int. Conf. Acoust., Speech, Signal Process.*, May 2001, vol. 6, pp. 3677-3680.
13. K. Chapman, *Building High Performance FIR Filters Using KCMs*. Xilinx Application Note, http://www.xilinx.com/appnotes/kcm_fir.pdf, 1996.
14. T. Hentschel and G. Fettweis, "Continuous-time digital filter for sample rate conversion in reconfigurable radio terminals," in *Proc. European Wireless Conf.*, pp. 55-59, June 1999.