

Analysis of Strength & Hardness of Weld Specimen of Mild-Steel Square Bars by Varying Arc Length and Voltage using Semi-Automatic Shielded Metal Arc Welding Machine

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ABSTRACT

Welding processes are widely used throughout industry to perform a range of fabrication tasks. Of the various welding techniques available, stick-electrode welding, more formally known as Shielded Metal Arc Welding (SMAW) is one of the most common. SMAW is a consumed electrode welding technique, i.e. the electrode not only supplies the filler-metal, but also acts as the consumable material. At present the feed rate of electrode is carefully controlled during the welding process to ensure that the arc length remains constant and Arc Voltage is also carefully controlled during the welding process by Voltage Regulator. The obtained results gives the Tensile Strength & Compressive Strength of the weld, and Weight of Specimen used when welding process is performed by varying Arc Length keeping the welding speed and arc voltage at constants. Also the results gives the Tensile Strength, Compressive Strength and Impact Strength of the weld, and Weight of specimen used when welding to constants. These parameters viz. Tensile Strength, Compressive Strength and Impact Strength of the weld work-piece is tested and recorded with the help of Tests performed in Universal Testing Machine viz. tensile test & compression test; and the Impact Strength of the weld is determined by Impact Testing Machine (ITM). This will be helpful in confirming the values of process parameters in SMAW. Later on, Hardness Test can be performed to determine the hardness of the weld by Rockwell Hardness Testing (RHT) Machine. The Results obtained is validated with the help of ANNOVA Test.

Keywords: SMAW – Shielded Metal Arc Welding, RHT Machine - Rockwell Hardness Test Machine, UTM - Universal Testing Machine, Process Parameters – Arc Gap, Arc Voltage, ITM – Impact Testing Machine

1. INTRODUCTION :

Welding processes are widely used throughout industry to perform a range of fabrication tasks. Of the various welding techniques available, stick-electrode welding, more formally known as Shielded Metal Arc Welding (SMAW) is one of the most common. SMAW is a consumed electrode welding technique, i.e. the electrode not only supplies the filler-metal, but also acts as the consumable material. Currently the electrode feed rate is carefully controlled during the welding process to ensure that the arc length remains constant. At present SMAW (Shielded Metal Arc Welding) process is done at fixed Voltage, fixed welding speed & fixed arc gap. This research work focuses light on measuring, recording and analyzing the variations in the weld strength and hardness of the weld if the fixed parameters would be changed within a given range. In this research, three process variable parameters are taken into account viz. arc voltage, welding speed & arc gap. This can be done by varying one of the process variable parameters and making the other two constants. Figure 1 illustrates the above statement diagrammatically. Result will be obtained for each and every varying process variable parameters and will be recorded. The obtained results will give the Tensile Strength & Compressive Strength of the weld, and Impact Strength and Hardness of the weld at varying arc gap and varying arc voltage. These parameters viz. Tensile Strength, Compressive Strength, Impact Strength & Hardness of the weld will help to conclude the result obtained individually at varying arc gap and at varying arc voltage conditions. The strength of the welds are tested and recorded in Universal Testing Machine viz. tensile test & compression test. The Toughness Test is tested and recorded in Impact Testing Machine using Charpy Test. Later on, Hardness Test is performed for determining the hardness of the weld by Rockwell Hardness Testing Machine. The results obtained in each case are validated by using ANNOVA Test in MS Excel Data Analysis Tool. This will be helpful in determining and confirming the exact and accurate values of process parameters in SMAW. Then the results obtained at varying arc gap and at varying arc voltage are compared and a conclusion is made.



Figure 1.1: Front View of Set up



Figure 1.1: Right Side View of Set up

Tensile and Compressive Strength of the weld is determined by UTM. The Toughness of the weld is determined by Impact Testing Machine.





2. LITERATURE REVIEW :

Patnaik et. al. (2007) [15] established a relationship between the controlling factors and performance outputs by means of Non-linear Regression Analysis and developed a valid mathematical model and Genetic Algorithm (GA) to optimize the welding parameter and performance output.

S Kumanan et. al. (2007) [16] worked on the application of Taguchi Technique and Regression Analysis to determine the optimal process parameters for SAW. They have carried out an experiment on a semi automatic submerged arc welding machine and the signals to noise ratios have been computed to determine the optimum parameters. The percentage contribution of each factor has been validated by ANOVA technique. Multiple regression analysis has also been carried out using SPSS software to develop mathematical models to predict the bead geometry for the given welding conditions. They also predicted the bead geometry from the developed model from the corresponding input data.

Chandel and Seow [17] presented the mathematical prediction of the effect of current, polarity used, electrode diameter and its extension on the melting rate, bead height, bead width and weld penetration in SAW. They concluded that for a given current (heat input) the melting rate can be increased by using electrode negative polarity, longer electrode extension, and smaller diameter electrodes. There are two other ways to increase the deposition rate without increasing the heat input; these are: (i) using a twin-arc mode and (ii) adding metal powders.

Chandel, Yang and Bibby [18] while investigating the effects of process variables on the bead width of submerged-arc weld deposits concluded that bead width is affected by the electrode polarity, electrode diameter, electrode extension, welding current, welding voltage and welding speed. A positive electrode polarity, a large electrode diameter, a small electrode extension and a high welding voltage encourages a large bead width in most cases. The bead width is not affected significantly by the power source used (i.e. constant voltage or constant current) when an acidic fused flux is used. However, when a basic fused flux is used, constant-current operation gives somewhat larger bead widths.

Mostafa and Khajavi [19] described the prediction of weld penetration as influenced by Flux Cored Arc Welding process parameters like welding current, arc voltage, nozzle-to-plate distance, electrode-to-work angle and welding speed. The optimization result shows penetration will be maximum when welding current, arc voltage, nozzle-to-plate distance and electrode-to- work angle are at their maximum possible value and welding speed is at its minimum value. Increase in welding current (I) increases the depth of penetration (P). Increase in welding speed (S) causes a decrease in depth of penetration (P). Increase in arc welding voltage (V) resulted in an increase in depth of penetration (P), Increase in electrode-to-work angle from 90° to 120° (i.e. for normal to backhand) had resulted in increase of depth of penetration. Increase in nozzle-to-plate distance (N) also causes an increase in depth of penetration (P). Based on this investigation it can be concluded that the developed model can be used to predict adequately the weld bead penetration within the specified range of the process parameters. The optimization method can also be used to find optimum welding conditions for maximum weld bead penetration. Their results are in agreement with the results of Chandel at. el.

Cheng-Yu Wu et al. (2008) [3] develops an automatic welding control scheme for alternating current shielded metal arc welding (SMAW) system. A mathematical model of the welding control system is derived and the system parameters identified. An adaptive sliding mode controller is designed to estimate the bound of the system uncertainties and to modulate the electrode feed rate in such a way that the desired arc length and arc current are maintained as the electrode melts during the welding process. The proposed control method is suitable for any consumed electrode welding technique. The simulation and experimental results show that the automatic welding control system successfully maintains the magnitude of the arc current at the desired value and preserves the arc stability, thereby obtaining an enhanced SMAW control system performance.

3. PROBLEM IDENTIFICATION :

The present situation in the field of SMAW (Shielded Metal Arc Welding) is that the whole welding process is done at fixed arc gap and fixed arc voltage. This research work focuses light on the effect on Strength and Hardness of the weld if the fixed arc gap and voltage is changed within a given range. In this research, the process variable parameter is taken into account is Arc Gap, Arc Voltage and Welding Speed. This can be done by in two ways. One way is by varying process variable parameter i.e. the Arc Gap and keeping Welding Speed and Arc Voltage at constant i.e. Welding Speed is kept constant at 5 mm.s-1 and Arc Voltage is kept constant at 30 Volt. And the other way is One way is by varying process variable parameter i.e. the Arc Voltage and keeping Welding Speed and Arc Gap at constant i.e. Welding Speed is kept constant at 5 mm.s-1 and Arc Voltage is kept constant at 30 Volt. Result will be obtained for each and every values of the process variable parameter ranging from 1.5 mm to 3.0 mm and will be recorded. The results will give the best possible values of Arc Gap and voltage at which welding can be performed with best possible Tensile Strength, Compressive Strength, Toughness and Hardness of the weld.

4. METHODOLOGY :



The Tensile Test & Compression Test is performed on Universal Testing Machine. And the Impact Test is performed on Impact Testing Machine. Hardness Test is performed on Rockwell Hardness Test Machine.

The Specimens used for the experimental analysis of Tensile & Compressive Strength of the weld are as follows:

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The Specimens used for the experimental analysis of Toughness of the weld are as follows:



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5. RESULT :

The welded work piece will be tested for tensile test, compression test & shear test with the help of Universal Testing Machine (UTM) to obtain the best Arc Gap at which Welding can be performed thus keeping the Welding Speed and Arc Voltage at constants i.e. Welding Speed is 5 mm.s-1 and Arc Voltage is 30 Volt, so that the Tensile Strength and Compressive Strength is at its best. Thus, when the results will be obtained, one will be able to find out the best possible Arc Gap for performing welding at which the Strength of the work-piece will be at its best. Individual Strength Charts are generated using the results among them at a given Arc Gap. Thus at each Arc Gap values considered for experimental analysis, Strength analysis is done and a Strength Chart is generated for the same so that the comparison among the strengths for a particular arc gap may be easily made.

Calculation of Mass of Specimen used in Kilogram:

Source: https://sites.google.com/site/standardbasicengineering/home/weights-ofround-square-hexagon-steel-brass-bars

| Table 5.1: Mass of Specimen used in Kilogram | | | | | | | |
|--|---------------------------------|--|----------------------------------|-----------------|---|--|--|
| Specimen No. | Weight of Steel (in Kg/m) | Thickness of Specimen (in mm) | Length of Specimen (in mm) | No. of Parts | Weight of Weld Specimen (in Kg.) | | |
| Specimen-1 | 0.283 | 6 | 150 | 2 | 0.5094 | | |
| Specimen-2 | 0.502 | 8 | 150 | 2 | 0.9036 | | |
| Specimen-3 | 0.785 | 10 | 150 | 2 | 1.143 | | |
| Specimen-4 | 1.130 | 12 | 150 | 2 | 2.034 | | |



Figure 5.1: Weight of Specimens (in Kg)

Calculations for Thickness and Cross-sectional Area of the Specimens:

The number of specimens used for the research is four viz., Specimen-1, Specimen-2, Specimen-3 and Specimen-4. The thickness and cross-sectional area of the four specimens is as follows:



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Table 5.2: Thickness and Cross-sectional Area of the Specimens

| | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 |
|---|------------|------------|------------|------------|
| Thickness of Specimen (in mm) | 6 | 8 | 10 | 12 |
| Cross-sectional Area (in mm ²) | 36 | 64 | 100 | 144 |



Figure 5.2: Graph for thickness and Cross-sectional area of the specimen

Result obtained by experimental analysis is as shown below: Table 5.3: Tensile Strengths of four specimens for Arc Gap Ranging from 1.5 mm to 3.0 mm :

| | | | Tensile Strengths (in MPa) | | | | |
|--------------------|--------|-----------|----------------------------|-----------|-----------|--|--|
| | | Specimen- | Specimen- | Specimen- | Specimen- | | |
| | | 1 | 2 | 3 | 4 | | |
| Arc Gap (in mm) | 1.5 mm | 91.5 | 95.3 | 103.5 | 110.5 | | |
| | 2.0 mm | 85.4 | 91.1 | 98.6 | 106.2 | | |
| | 2.5 mm | 63.2 | 72 | 77.4 | 83.6 | | |
| | 3.0 mm | 45.5 | 50.2 | 58.2 | 68.7 | | |

Arc Voltage = 30 V, Welding Current = 110 A, Welding Speed = 5 mm.s⁻¹



Figure 5.3: Graph for Tensile Strengths of four specimens for Arc Gap Ranging from 1.5 mm to 3.0 mm

Table 5.4: Compressive Strengths of four specimens for Arc Gap Ranging from 1.5 mm to 3.0 mm :

| | | Compressive Strengths (in MPa) | | | | | |
|--|-----------|--------------------------------|-------|-------|-------|--|--|
| Specimen-1 Specimen-2 Specimen-3 Specimen- | | | | | | | |
| | 1.5 mm | 105.4 | 113.4 | 120.2 | 132.4 | | |
| Arc Gap | 2.0 mm | 99.2 | 107.5 | 102.2 | 109.5 | | |
| (in mm) | 2.5 mm | 81 | 89.6 | 95.8 | 102.8 | | |
| | 3.0 mm | 69.3 | 76.4 | 82.3 | 91.3 | | |





Figure 5.4: Graph for Compressive Strengths of four specimens for Arc Gap Ranging from 1.5 mm to 3.0 mm

| Table 5.5: Impact Energy of four specimens for Arc Gap | Ranging from 1.5 |
|--|------------------|
| mm to 3.0 mm | |

| | | Impact Energy (in Joule) | | | | |
|--------------------|--------|--------------------------|------------|------------|------------|--|
| | | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 | |
| Arc Gap (in mm) | 1.5 mm | 10.2 | 12.8 | 14.0 | 16.5 | |
| | 2.0 mm | 9.0 | 10.4 | 11.2 | 12.9 | |
| | 2.5 mm | 6.6 | 8.7 | 9.3 | 10.7 | |
| | 3.0 mm | 5.3 | 7.5 | 7.2 | 8.1 | |

| Arc Voltage = 30 V, Welding Current = 110 A, Welding Speed = 5 mm.s | -1 |
|---|----|
|---|----|



Figure 5.5: Graph for Impact Energy of four specimens for Arc Gap Ranging from 1.5 mm to 3.0 mm

| Table 5.6: Impact Strength of four specimens for Arc Gap Ranging from 1.5 |
|---|
| mm to 3.0 mm |

| | | Impact Strength (in KJ/m ²) | | | | |
|--------------------|--------|---|------------|------------|------------|--|
| | | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 | |
| | 1.5 mm | 283.33 | 200.00 | 140.00 | 114.58 | |
| Arc Gap (in mm) | 2.0 mm | 250.00 | 162.50 | 112.00 | 89.58 | |
| | 2.5 mm | 183.33 | 135.93 | 93.00 | 74.30 | |
| | 3.0 mm | 147.22 | 117.18 | 72.00 | 56.25 | |

Arc Voltage = 30 V, Welding Current = 110 A, Welding Speed = 5 mm.s⁻¹



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Figure 5.6: Graph for Impact Strength of four specimens for Arc Gap Ranging from 1.5 mm to 3.0 mm

Table 5.7: Hardness of four specimens for Arc Gap ranging from 1.5 mm to 3.0 mm obtained by Testing in Rockwell Hardness Testing Machine

Arc Voltage = 30 V Welding Current = 110 A Welding Speed = 5 mm.s^{-1} Applied Load= 250 Kgf Penetrator Type = Diamond Cut (Code used is C) Hardness Test Method: Rockwell Hardness Test Method (Code used is HR)

| | | Hardness of Weld Specimen | | | |
|---------|--------|---------------------------|------------|------------|------------|
| | | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 |
| | 1.5 mm | HRC 28 | HRC 37 | HRC 36 | HRC 36 |
| Arc Gap | 2.0 mm | HRC 27 | HRC 35 | HRC 34 | HRC 34 |
| (in mm) | 2.5 mm | HRC 24 | HRC 32 | HRC 31 | HRC 31 |
| | 3.0 mm | HRC 20 | HRC 30 | HRC 28 | HRC 30 |



Figure 5.7: Graph for Rockwell Hardness of four specimens for Arc Gap ranging from 1.5 mm to 3.0 mm

Table 5.8: Tensile Strengths of four specimens for Arc Voltage Ranging from 25 Volt to 40 Volt :

| | | Tensile Strengths (in MPa) | | | |
|----------------------------|---------|----------------------------|----------------|----------------|----------------|
| Specimen Specimen- -1 2 | | | Specimen- 2 | Specimen- 3 | Specimen- 4 |
| Arc | 25 Volt | 109.7 | 112.6 | 118.0 | 125.5 |
| Voltage | 35 Volt | 91.5 | 95.3 | 103.5 | 110.5 |
| (in Volt) | 35 Volt | 89.5 | 91.4 | 100.8 | 106.8 |
| | 40 Volt | 85.6 | 89.0 | 94.2 | 97.3 |

Arc Gap = 1.5 mm, Welding Current = 110 A, Welding Speed = 5 mm.s^{-1}



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Figure 5.8: Graph for Tensile Strengths of four specimens for Arc Voltage Ranging from 25 Volt to 40 Volt

Table 5.9: Compressive Strengths of four specimens for Arc Voltage Ranging from 25 Volt to 40 Volt :

| | | Compressive Strengths (in MPa) | | | | |
|-----------------------------|---------|--------------------------------|------------|------------|------------|--|
| | | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 | |
| | 25 Volt | 109.2 | 116.1 | 127.3 | 138.6 | |
| Arc Voltage (in Volt) | 30 Volt | 105.4 | 113.4 | 120.2 | 132.4 | |
| | 35 Volt | 99.1 | 102.3 | 105.2 | 108.5 | |
| | 40 Volt | 71.2 | 72.9 | 94.6 | 97.5 | |





Figure 5.9: Graph for Compressive Strengths of four specimens for Arc Voltage Ranging from 25 Volt to 40 Volt

| Table 5.10: Impact Energy of four specimens for Arc Voltage | Ranging from |
|---|--------------|
| 25 Volt to 40 Volt | |

| | | Impact Energy (in Joule) | | | |
|---|---------|--------------------------|------------|------------|------------|
| | | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 |
| Arc Voltage (in Volt) 25 Volt 30 Volt 35 Volt 40 Volt | 25 Volt | 12.0 | 13.8 | 16.0 | 18.4 |
| | 30 Volt | 10.2 | 12.8 | 14.0 | 16.5 |
| | 35 Volt | 8.4 | 9.7 | 11.3 | 12.6 |
| | 40 Volt | 7.1 | 8.5 | 9.2 | 10.0 |

Arc Gap = 1.5 mm, Welding Current = 110 A, Welding Speed = 5 mm.s^{-1}



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Figure 5.10: Graph for Impact Energy of four specimens for Arc Voltage Ranging from 25 Volt to 40 Volt

Table 5.11: Impact Strength of four specimens for Arc Voltage Ranging from 25 Volt to 40 Volt:

| | | Impact Strength (in KJ/m ²) | | | |
|----------------|---------|---|------------|------------|------------|
| | | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 |
| | 25 Volt | 333.33 | 215.62 | 160.00 | 127.77 |
| Arc Voltage | 30 Volt | 283.33 | 200.00 | 140.00 | 114.58 |
| (in Volt | 35 Volt | 233.33 | 151.56 | 113.00 | 87.50 |
| | 40 Volt | 197.22 | 132.81 | 92.00 | 69.44 |

Arc Gap = 1.5 mm, Welding Current = 110 A, Welding Speed = 5 mm.s^{-1}



Figure 5.11 Graph for Impact Strength of four specimens for Arc Voltage Ranging from 25 Volt to 40 Volt



Arc Voltage = 30 V Welding Current = 110 A Welding Speed = 5 mm.s^{-1} Applied Load= 250 Kgf Penetrator Type = Diamond Cut (Code used is C) Hardness Test Method: Rockwell Hardness Test Method (Code used is HR

| | | Hardness of Weld Specimen | | | |
|--------------------------|---------|---------------------------|------------|------------|------------|
| | | Specimen-1 | Specimen-2 | Specimen-3 | Specimen-4 |
| Arc Voltage (in Volt) | 25 Volt | HRC 30 | HRC 39 | HRC 37 | HRC 37 |
| | 30 Volt | HRC 28 | HRC 36 | HRC 35 | HRC 35 |
| | 35 Volt | HRC 25 | HRC 33 | HRC 32 | HRC 31 |
| | 40 Volt | HRC 22 | HRC 31 | HRC 30 | HRC 30 |





CONCLUSION :

From the result and graph obtained by comparing the four specimens Tensile & Compressive strengths and weight of the specimen for Arc Gap ranging from 1.5 mm to 3.0 mm, made by welding Mild Steel Square Bar (Specimen Thickness x 150 mm Length) x 2 Nos. welded at the centre (keeping Arc Voltage & welding Speed at constants); and from the result and graph obtained by comparing the four specimens Tensile & Compressive strengths for Arc Voltage ranging from 25 Volt to 40 volt, made by welding Mild Steel Square Bar (Specimen Thickness x 150 mm Length) x 2 Nos. welded at the centre (keeping Arc Gap & welding Speed at constants), the conclusions made are as follows:

- 1. The Tensile Strength of the weld decreases with increase in Arc Gap & Arc Voltage whereas Tensile Strength increases with decreases in Arc Gap & Arc Voltage. Also, The Tensile Strength of the weld increases with increase in thickness or weight of the specimen whereas Tensile Strength decreases with decrease in thickness or weight of the specimen.
- 2. The Compressive Strength of the weld decreases with increase in Arc Gap & Arc Voltage whereas Compressive Strength increases with decreases in Arc Gap & Arc Voltage. Also, The Compressive Strength of the weld increases with increase in thickness or weight of the specimen whereas Compressive Strength decreases with decrease in thickness or weight of the specimen.
- 3. The Impact Energy of weld decreases with increase in Arc Gap & Arc Voltage whereas the Impact Energy of weld increases with decrease in Arc Gap & Arc Voltage. The Impact Energy of the weld increases with increase in thickness or weight of the specimen whereas Impact Energy of the weld decreases with decrease in thickness or weight of the specimen.
- 4. The Impact Strength of weld decreases with increase in Arc Gap & Arc Voltage whereas the Impact Strength of weld increases with decrease in Arc Voltage. Also, The Impact Strength of the weld decreases with increase in thickness or weight of the specimen whereas Impact Strength of the weld increases with decrease in thickness or weight of the specimen.
- 5. The Hardness of the weld decreases with increase in Arc Gap & Arc Voltage whereas the hardness of the weld increases with decrease in Arc Gap & Arc Voltage. Also, Hardness of the weld first increases then slightly decreases with increase in thickness & weight of the specimen whereas the hardness of the weld first slightly increases then decreases with decrease in thickness & weight of the specimen

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VALIDATION:

Validation of the result obtained is done with the help of ANNOVA Test using MS Excel Data analysis Tool.

Anova: Two-Factor With Replication

| 10110110 001 0 | <u>Specimen-1</u> ngth (in Mpa) of | Specimen-2 Weld at Arc Gap | Specimen-3 | Specimen-4 | Total |
|---|---|---|---|---|---|
| Count | 4 | 4 | 4 | 4 | 16 |
| Sum | 285.6 | 308.6 | 337.7 | 369 | 1300.9 |
| Average | 71.4 | 77.15 | 84.425 | 92.25 | 81.30625 |
| Variance | 446.02 | 425.6167 | 433.9625 | 385.6967 | 403.566 |
| Comnressiv | e Strenath (in M | pa) of Weld at Ar | rc Gap 1.5 mm | | |
| Count | 4 | 4 | 4 | 4 | 16 |
| Sum | 354.9 | 386.9 | 400.5 | 436 | 1578.3 |
| Average | 88.725 | 96.725 | 100.125 | 109 | 98.64375 |
| Variance | 274.9292 | 286.0092 | 247.9158 | 299.8467 | 278.1426 |
| Impact Ener | ray (in loules) of | Weld at Arc Gap | 15 mm | | |
| Count | <u>4</u> | 4 | 4 | 4 | 16 |
| Sum | 31.1 | 39.4 | 41.7 | 48.2 | 160.4 |
| Average | 7.775 | 9.85 | 10.425 | 12.05 | 10.025 |
| Variance | 4.9625 | 5.283333 | 8.349167 | 12.65 | 8.743333 |
| / | n anth (in 1/1/10.2) | of World at Are C | | | |
| <i>Impact Stre</i> Count | <u>ngth (in KJ/m2) (</u> 4 | o <u>f Weld at</u> Arc Go 4 | <u>ap 1.5 mm</u> 4 | 4 | 16 |
| Sum | 4 863.88 | 4 615.61 | 4 417 | 4 334.71 | 2231.2 |
| Average | 215.97 | 153.9025 | 104.25 | 83.6775 | 139.45 |
| Variance | 3829.114 | 1290.15 | 834.9167 | 610.0031 | 4089.849 |
| variance | 5625.114 | 1250.15 | 004.0107 | 510.0051 | +000.045 |
| | ^F Weld at Arc Ga | | | | |
| Count | 4 99 | 4 134 | 4 129 | 4 131 | 16 493 |
| Sum | 99 24.75 | | | 131 32.75 | |
| Average | | 33.5 | 32.25 | | 30.8125 |
| Variance | 12.91667 | 9.666667 | 12.25 | 7.583333 | 21.7625 |
| <u>Tensile Stre</u> | ngths (in MPa) a | t 25 Volt | | | |
| Count | 4 | 4 | 4 | 4 | 16 |
| Sum | 376.3 | 388.3 | 416.5 | 440.1 | 1621.2 |
| Average | 94.075 | 97.075 | 104.125 | 110.025 | 101.325 |
| Variance | 114.5092 | 113.8625 | 100.8225 | 137.3425 | 134.4153 |
| Compressiv | e Strengths (in N | APa) at 25 Volt | | | |
| Compressiv Count | <u>e strengtns (in N</u> 4 | <u>4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 </u> | 4 | 4 | 16 |
| Sum | 4 447.5 | 4 474.1 | 4 475.7 | 4 496.8 | 1894.1 |
| Average | 111.875 | 118.525 | 118.925 | 124.2 | 118.3813 |
| Variance | 99.7225 | 57.44917 | 134.9492 | 124.2 | 104.351 |
| | | | | | |
| | r <u>qy (in Joules) at</u> | | ٨ | 4 | 16 |
| Count Sum | 4 43.4 | 4 49.7 | 4 49.7 | 4 55.8 | 16 198.6 |
| Julli | | 49.7 12.425 | 49.7 12.425 | | |
| Avorage | 10 QE | 12.425 | 12.425 | 13.95 | 12.4125 |
| | 10.85 5.283333 | | 8.349167 | 12.65 | |
| Average Variance | 10.85 5.283333 | 8.349167 | 8.349167 | 12.65 | |
| Variance Impact Stre | 5.283333 ngth (in KJ/m2) | 8.349167 at 25 Volt | | | 8.207833 |
| <i>Impact Stre</i> Count | 5.283333 ngth (in KJ/m2) 4 | 8.349167 at 25 Volt 4 | 4 | 4 | 8.207833 |
| Variance Impact Stre Count Sum | 5.283333 ngth (in KJ/m2) 4 1063.88 | 8.349167 at 25 Volt 4 678.11 | 4 497 | 4 387.48 | 8.207833 16 2626.47 |
| Variance Impact Stre Count Sum Average | 5.283333 ngth (in KJ/m2) 4 1063.88 265.97 | 8.349167 at 25 Volt 4 678.11 169.5275 | 4 497 124.25 | 4 387.48 96.87 | 8.207833 16 2626.47 164.1544 |
| Variance Impact Stre Count Sum Average | 5.283333 ngth (in KJ/m2) 4 1063.88 | 8.349167 at 25 Volt 4 678.11 | 4 497 | 4 387.48 | 8.207833 16 2626.47 164.1544 |
| Variance Impact Stre Count Sum Average Variance | 5.283333 ngth (in KJ/m2) 4 1063.88 265.97 | 8.349167 at 25 Volt 4 678.11 169.5275 1289.785 | 4 497 124.25 834.9167 | 4 387.48 96.87 | 8.207833 16 2626.47 164.1544 5716.708 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count | 5.283333 nath (in KJ/m2) + 4 1063.88 265.97 3829.114 <u>F Weld at 25 Vol</u> 4 | 8.349167 <i>at 25 Volt</i> 4 678.11 169.5275 1289.785 <i>t</i> 4 | 4 497 124.25 834.9167 4 | 4 387.48 96.87 609.9406 4 | 8.207833 16 2626.47 164.1544 5716.708 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum | 5.283333 ngth (in KJ/m2) + 4 1063.88 265.97 3829.114 F Weld at 25 Vol 4 105 | 8.349167 <i>at 25 Volt</i> 4 678.11 169.5275 1289.785 <i>t</i> 4 139 | 4 497 124.25 834.9167 4 134 | 4 387.48 96.87 609.9406 4 133 | 8.207833 16 2626.47 164.1544 5716.708 16 511 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 f Weld at 25 Vol 4 105 26.25 | 8.349167 at 25 Volt 4 678.11 169.5275 1289.785 t 4 139 34.75 | 4 497 124.25 834.9167 4 134 33.5 | 4 387.48 96.87 609.9406 4 133 33.25 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average | 5.283333 ngth (in KJ/m2) + 4 1063.88 265.97 3829.114 F Weld at 25 Vol 4 105 | 8.349167 <i>at 25 Volt</i> 4 678.11 169.5275 1289.785 <i>t</i> 4 139 | 4 497 124.25 834.9167 4 134 | 4 387.48 96.87 609.9406 4 133 | 8.207833 16 2626.47 164.1544 5716.708 16 511 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 f Weld at 25 Vol 4 105 26.25 | 8.349167 at 25 Volt 4 678.11 169.5275 1289.785 t 4 139 34.75 | 4 497 124.25 834.9167 4 134 33.5 | 4 387.48 96.87 609.9406 4 133 33.25 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 f Weld at 25 Vol 4 105 26.25 | 8.349167 at 25 Volt 4 678.11 169.5275 1289.785 t 4 139 34.75 | 4 497 124.25 834.9167 4 134 33.5 | 4 387.48 96.87 609.9406 4 133 33.25 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count | 5.283333 nath (in KJ/m2) + 4 1063.88 265.97 3829.114 f Weld at 25 Vol 4 105 26.25 12.25 | 8.349167 <i>at 25 Volt</i> <i>4</i> 678.11 169.5275 1289.785 <i>t</i> <i>4</i> 139 34.75 12.25 | 4 497 124.25 834.9167 4 134 33.5 9.666667 | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count Sum | 5.283333 nath (in KJ/m2) + 4 1063.88 265.97 3829.114 <i>Weld at 25 Vol</i> 4 105 26.25 12.25 40 3670.56 | 8.349167 at 25 Volt 4 678.11 169.5275 1289.785 t 4 139 34.75 12.25 40 3213.72 | 4 497 124.25 834.9167 4 134 33.5 9.666667 40 2898.8 | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 40 2832.09 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count Sum Average | 5.283333 nath (in KJ/m2) + 4 1063.88 265.97 3829.114 <i>Weld at 25 Vol</i> 4 105 26.25 12.25 40 | 8.349167 <i>at 25 Volt</i> 4 678.11 169.5275 1289.785 <i>t</i> 4 139 34.75 12.25 40 | 4 497 124.25 834.9167 4 134 33.5 9.6666667 40 | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 40 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count Sum Average Variance | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 <i>Weld at 25 Vol</i> 4 105 26.25 12.25 40 3670.56 91.764 | 8.349167 <u>4</u> 678.11 169.5275 1289.785 <u>1289.785</u> <u>t</u> <u>4</u> 139 34.75 12.25 <u>40</u> 3213.72 80.343 | 4 497 124.25 834.9167 4 134 33.5 9.666667 40 2898.8 72.47 | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 40 2832.09 70.80225 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count Sum Average Variance ANOVA | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 <i>Weld at 25 Vol</i> 4 105 26.25 12.25 40 3670.56 91.764 7739.937 | 8.349167 4 678.11 169.5275 1289.785 <i>it</i> 4 139 34.75 12.25 40 3213.72 80.343 3267.712 | 4 497 124.25 834.9167 4 134 33.5 9.666667 40 2898.8 72.47 2084.085 | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 40 2832.09 70.80225 1882.765 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count Sum Average Variance AnovA | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 <i>Weld at 25 Vol</i> 4 105 26.25 12.25 40 3670.56 91.764 | 8.349167 <u>4</u> 678.11 169.5275 1289.785 <u>1289.785</u> <u>t</u> <u>4</u> 139 34.75 12.25 <u>40</u> 3213.72 80.343 | 4 497 124.25 834.9167 4 134 33.5 9.666667 40 2898.8 72.47 2084.085 df | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 40 2832.09 70.80225 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count Sum Average Variance ANOVA | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 <i>Weld at 25 Vol</i> 4 105 26.25 12.25 40 3670.56 91.764 7739.937 | 8.349167 4 678.11 169.5275 1289.785 <i>t</i> 4 139 34.75 12.25 40 3213.72 80.343 3267.712 | 4 497 124.25 834.9167 4 134 33.5 9.666667 40 2898.8 72.47 2084.085 | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 40 2832.09 70.80225 1882.765 | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 20.8625 |
| Variance Impact Stre Count Sum Average Variance Hardness of Count Sum Average Variance Total Count Sum Average Variance AnovA Source | 5.283333 nath (in KJ/m2) (4 1063.88 265.97 3829.114 <i>Weld at 25 Vol</i> 4 105 26.25 12.25 40 3670.56 91.764 7739.937 | 8.349167 <u>4</u> 678.11 169.5275 1289.785 <u>1289.785</u> <u>4</u> 139 34.75 12.25 <u>40</u> 3213.72 80.343 <u>3267.712</u> | 4 497 124.25 834.9167 4 134 33.5 9.666667 40 2898.8 72.47 2084.085 df | 4 387.48 96.87 609.9406 4 133 33.25 10.91667 40 2832.09 70.80225 1882.765 <i>MS</i> | 8.207833 16 2626.47 164.1544 5716.708 16 511 31.9375 20.8625 8 |

| Within | 50902.7935 | 120 | 424.189946 |
|---------------------|------------|------------|------------|
| Total | 594984.3 | 159 | |
| | | | |
| Source of Variation | F | P-value | F crit |
| Sample | 113.467295 | 2.2738E-54 | 1.9587633 |
| Columns | 8.62729916 | 3.1274E-05 | 2.68016758 |
| Interaction | 8.72403489 | 1.1848E-17 | 1.57892389 |

Results obtained after ANNOVA Test:

Define Alternative Hypothesis: *Alternate Hypothesis:* All the values of parameters obtained by experimental analysis are correct and can be used for the research.

i.e., $H_1: \mu \le 0.05$

Define Null Hypothesis: *Null Hypothesis:* All the values of parameters obtained are not appropriate and needs to be corrected.

i.e., $H_0:\mu > 0.05$

F (Sample) = 113.467295, F-crit (Sample) = 1.9587633 Therefore, F (Sample) > F-crit (Sample)Equation (i)

F (Columns) = 8.62729916, F-crit (Columns) = 2.68016758 Therefore, F (Columns) > F-crit (Columns)Equation (ii)

| F (Interaction) = 8.72403489, F-crit (Inter Therefore, F (Interaction) > F-crit (Interaction) | , | 1.57892389 Equation (iii) |
|--|--------------|------------------------------|
| P (Sample) = 2.2738E-54 > α (= 0.05) | | Equation (iv) |
| Also, P (Columns) = $3.1274E-05 > \alpha$ (= 0. | 05) | Equation (v) |
| Also, P (Interaction) = $1.1848E-17 > \alpha$ (= | 0.05) | Equation (vi) |
| From Equation (i), (ii) and (iii); | F > F-crit | |
| From Equation (iv), (v) and (vi); | P > a | |
| Therefore, Null Hypothesis (H_0 : $\mu > 0.05$) | is rejected. | |

And hence; Alternate Hypothesis i.e. $(H_1: \mu \le 0.05)$ is selected.

Therefore, It is concluded that, "All the values of parameters obtained by experimental analysis are correct and can be used for the research". Hence, Result is validated.

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