

Computational and Experimental Investigation & Analysis on the Effect of Milled Basalt Fibre Fillers on Static Flexural Properties of the Natural Fibre Composites for Aerospace and Automobile Industrial Applications

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Abstract - Academic and industry researchers are focused on developing a material that satisfies various parameters such as durability, manufacturability, low cost, lightweight, adaptability, high strength, bio-degradability, etc. to meet the current day trends across aerospace and automotive industries. In engineering and technology, fiber-reinforced matrix composites and their applications are extensive. The addition of fillers (both natural and synthetic) along with matrix and fibers is considered to be a better option to increase the efficiency and performance of the composite materials. Recently, researchers have focussed on adding fillers along with matrix and its hybridization to lift the composite properties and applications. This research paper describes the computational and experimental investigation & analysis on the effect of milled basalt fibre fillers on static flexural properties of the natural fibre composites for aerospace and automobile applications. As a first step, an optimized milled filler percentage is examined by incorporating the basalt milled filler into the epoxy laminates from 0.5% to 3% weight percentages concerning epoxy laminates. Finally, the 1% filler incorporated epoxy laminates showed better results than the base samples. Then, the 1% milled basalt filler material was incorporated into basalt fiber and areca fiber with epoxy resin and hardener to make the composite laminates for static testing. The static testing was carried out with the help of a Universal Testing Machine (UTM) i.e. the three-point bending test. The filler-incorporated basalt and areca nut epoxy composite laminates show higher flexural properties than the base samples with 0% filler material. The project work was also carried out with the help of ANSYS software with proper filler material and epoxy composite laminates for static testing. The flexural properties of the filler-incorporated composite laminates show higher properties than the base samples. Results reveal that the flexural properties of the composite laminates from experimental testing and software analysis are of less error percentage difference.

Key Words: Composite materials & structures, Matrix, Fibres, Fillers, Mechanical properties, Static testing, Flexural properties and ANSYS

1. INTRODUCTION

As discussed in the abstract, composite materials and structures are major research areas that are well-suited for aerospace and automotive applications. Generally, composites are cheaper and have a good strength-to-weight ratio. Recent day researchers have focused greatly on developing a material with matrix and fiber along with fillers (either natural or synthetic). The addition of fillers influences the mechanical properties of the composite materials significantly. To prepare

a material that satisfies various properties and to enhance mechanical properties, the filler addition to the matrix and hybridization of fibers are a better option. This review paper briefly describes only the addition of fillers to the mechanical properties of a composite material. The filler addition influences the properties of the composites which depends on the filler size, shape, aspect ratio, surface area, etc. to meet the current trends of the material for the engineering applications.

The addition of fillers to the matrix enhances properties and processability and reduces the cost of material. The fillers may be micro or nano-sized particles. From the various research studies, it is concluded that the use of nanosized filler would be an ideal option to improve properties as nano-sized particles are characterized by as high aspect ratio and specific surface area. The interaction between the polymer fiber and matrix increases with the addition of an optimum composition of fillers. After a certain limit of addition of fillers results in decreased properties because the agglomerations of the fillers take place. Hence, the application of nanofillers within the polymer matrix is an extensive research area in the field of engineering and technology.

Natural fibers are environment friendly, as it is biodegradable, and good recyclability. They are cheaper than conventional synthetic fibers. They are abundant in nature, and renewable, causing low risk to human health. Composites replace conventional materials like steel, aluminum, etc in most of the aircraft components due to their high strength-to-weight ratio. But almost all synthetic fibers are used in aerospace due to their higher strength than natural ones, and for safety. However, by using milled fillers of natural fibers, we try to improve the strength of natural fiber composite up to about 70-80% of that of synthetic fibers, so that natural fiber composites may be incorporated in aircraft components shortly. The damaged or utilized composites can be treated appropriately (mechanically, chemically, or thermally to extract the fibers alone to be used as fillers in new composite laminates, as these fibers can be milled (powdered/chopped), and used as fillers to enhance the mechanical properties of the composites.

Generally, the addition of fillers along with resin and fiber improves mechanical properties. Including fillers in the interlayer enhances the delamination resistance by providing a bridging effect, therefore demanding additional energy to initiate the crack in the interlaminar domain, which results in turn in enhanced fracture toughness. The mechanism observed suggests that crack propagation is stabilized even leading to its arrest/deflection, as a considerable amount of milled fiber filler was oriented transverse to the crack path. In contrast, at higher filler loading, a tendency towards stress concentration grows due to local agglomeration and improper dispersion of excess fillers in inter/intralaminar resin channel, causing poor adhesion to the matrix, which leads to a reduction in fracture

toughness, and strength and strain to failure. This research paper describes the computational and experimental investigation & analysis on the effect of milled basalt fibre fillers on static flexural properties of the natural fibre composites for aerospace and automobile applications.

1.1 Composite: An Overview

A composite is a structural material that consists of two or more combined constituents that are combined at a macroscopic level and are not soluble in each other. One constituent is called the reinforcing phase and the one in which it is embedded is called the matrix. The reinforcing phase material may be in the form of fibers, particles, or flakes. The matrix phase materials are generally continuous. Examples of composite systems include concrete reinforced with steel and epoxy reinforced with graphite fibers, etc. Advanced composites are composite materials that are traditionally used in the aerospace industries. These composites have high-performance reinforcements of a thin diameter in a matrix material such as epoxy and aluminum. Examples are graphite/epoxy, Kevlar R/epoxy, and boron/aluminum composites. These materials have now found applications in commercial industries as well. Fiber composites consist of matrices reinforced by short (discontinuous) or long (continuous) fibers. Fibers are generally anisotropic, and examples include carbon and aramids. Examples of matrices are resins such as epoxy, metals such as aluminum, and ceramics such as calcium-aluminum silicate. Composites are strong but lightweight, making them ideal for creating lighter products. They are also resistant to harsh weather conditions, chemicals, and fuels, as well as corrosion and wear, and usually don't need special anti-corrosion treatment. Composites can be molded into complex shapes and structures. Composites require little maintenance once installed. Composites can insulate against electricity and heat. Composites can absorb and withstand impacts. Composites can improve fuel efficiency in transportation. Composites can be made in a wide range of colors. Composites can be easily repaired.

Synthetic fibers are non-biodegradable and are more expensive than Natural fibers. They cause environmental degradation and have moderate recyclability. Natural fibers are environment friendly, as it is biodegradable, and have good recyclability. They are cheaper than conventional synthetic fibers. They are abundant in nature, and renewable, causing low risk to human health. Composites replace conventional materials like steel, aluminum, etc in most of the aircraft components due to their high strength-to-weight ratio. But almost all synthetic fibers are used in aerospace due to their higher strength than natural ones, and for safety. However, by using milled fillers of natural fibers, we try to improve the strength of natural fiber composite up to about 70-80% of that of synthetic fibers, so that natural fiber composites may be incorporated in aircraft components shortly. The damaged or utilized composites can be treated appropriately (mechanically, chemically, or thermally to extract the fibers alone to be used as fillers in new composite laminates, as these fibers can be milled (powdered/chopped), and used as fillers to enhance the mechanical properties of the composites, which is carried out exactly in this project work.

1.2 Epoxy Resins

Epoxy resins are the most used resins. They are low molecular weight organic liquids containing epoxide groups. Epoxide has three members in its ring: one oxygen and two carbon atoms. The reaction of epichlorohydrin with phenols or aromatic amines makes most epoxies. Hardeners, plasticizers, and fillers are also added to produce epoxies with a wide range of properties of viscosity, impact, degradation, etc. Although epoxy is costlier than other polymer matrices, it is the most popular PMC matrix. More than two-thirds of the polymer matrices used in aerospace applications are epoxy-based. The main reasons why epoxy is the most used polymer matrix material are High strength, Low viscosity, and low flow rates, which allow good wetting of fibers and prevent misalignment of fibers during processing, low volatility during cure Low shrink rates, which reduce the tendency of gaining large shear stresses of the bond between epoxy and its reinforcement and available in more than 20 grades to meet specific property and processing requirements.

1.3 Significance of Natural Fillers

Filler materials are particles added to resin or binders (plastics, composites, concrete) that can improve specific properties of composite material. These can be milled or chopped fibers, which form good bonding with resin material, improve its mechanical, and thermal properties, and prevent crack propagation. The current demand for high-performance green composites has resulted in the use of natural fillers as a reinforcement in the epoxy matrix, which is also a means of recycling. The need to utilize green materials for a sustainable environment has caused an upsurge in the use of natural materials in the composite industry because the sustainability of the products during processing and end-of-life is important. Natural fillers are sustainable potential materials as reinforcing agents for different polymer matrices in varying applications such as automobile, construction, aerospace, toys, defense, sporting goods, and electronic applications. The other advantages of natural fibers are their easy availability, easy manufacturing process, less energy consumption, renewability, and good mechanical properties. These advantages make natural fillers an alternative to traditional fillers in many applications such as construction and infrastructure, furniture, and rotor blade materials. Plant-based fillers such as banana fiber, hemp, sisal, pineapple, bamboo, flax, peanut particles, etc., have been widely used as reinforcement for various polymer matrices. Studies have shown that plant fibers are an excellent replacement for carbon and glass fibers in many semi-structural applications. Filler materials come in a few diverse forms: glass beads, short glass fibers, and long glass fibers. In plastics by tonnage. Glass fiber fillers are used to increase the mechanical properties of the thermoplastic or thermoset such as flexural modulus and tensile strength. There is normally no economic benefit to adding glass as a filler material. Some disadvantages of having glass in the matrix include low surface quality, high viscosity when melted, poor weldability, and warpage. Hence there has been much research carried out using natural fillers. For, example Abdelmalik et al. studied the variations in tensile strength and insulation properties of the epoxy composites with the addition of eggshell powder in which he observed that the tensile strength of epoxy composites was increased with the increasing addition of eggshell powder, and the best results were observed for 4 wt%

filler, which was followed by a reduction for the composite with 5% filler content due to the agglomeration of the particles. With these scopes of using natural fillers, we have chosen Basalt and Arecanut fibers and fillers, to be incorporated in epoxy resin.

1.4 Three Point Bending Test

The three-bending test is a widely used method in structural analysis to evaluate the mechanical properties and strength of materials. It involves applying a load to a specimen that is supported at two points while a third point applies the force. This test is particularly useful in determining the flexural strength and stiffness of materials. During the test, the specimen is placed horizontally on two supports, with a loading point positioned at the center. A force is then applied downward on the loading point, causing the specimen to bend. As the load increases, the specimen undergoes deformation, and the resulting stress and strain distribution along its length are measured.

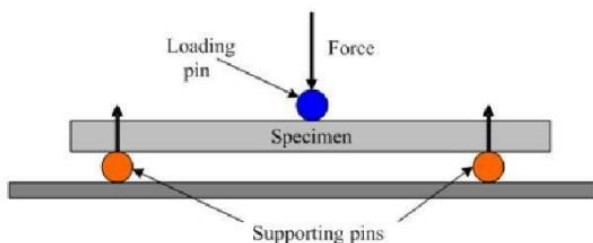


Figure 1: Three Point Bending Test

One of the key advantages of the three-point bending test is its ability to simulate real-world conditions, as many structural elements experience bending loads in practical applications. This test provides valuable information about a material's ability to withstand bending forces and its resistance to fracture. By analyzing the stress-strain relationship obtained from the three-point bending test, several important material properties such as modulus of elasticity, yield strength, ultimate strength, and fracture toughness can be determined. This information is crucial for designing and assessing the structural integrity of various components such as beams, columns, and other load-bearing elements.

2. LITERATURE SURVEY

[1] G.L. Devnani, Shishir Sinha. Effect of nanofillers on the properties of natural fiber reinforced polymer composites. *ScienceDirect Materials Today: Proceedings* 18 (2019) 647–654 ICN3I-2017

Investigation of the effect of nanofillers on the mechanical properties of fiber-reinforced polymer composites. The addition of nanofillers influences the mechanical properties and water absorption properties. To keep a balance in terms of properties, it is evident to use the optimum composition of filler material to improve properties significantly. Various nanofibers are used as fillers such as granite, nano-Sio₂, CNT, graphene, etc.

[2] Vikas Dhawan, Sehijpal Singh and Inderdeep Singh. Effect of Natural Fillers on Mechanical Properties of

GFRP Composites. Hindawi Publishing Corporation. *Journal of Composites*. Volume 2013, Article ID 792620, 8 pages <http://dx.doi.org/10.1155/2013/792620>

This paper briefly presents the effect of natural fillers on the mechanical properties of the GFRP composites. The natural fillers used are rice husk, wheat husk, and coconut coir. The matrix materials used along with GFRP are polyester and epoxy resins. The addition of fillers leads to the cost and weight reduction of the glass fiber-reinforced composites. From the paper, we found that the natural fillers with polyester-based composites provide better results than the epoxy-based composites. Water absorption is more in polyester-based composites. In general, we infer that to improve the properties of the GFRP, coconut coir fillers should be used instead of rice husk and wheat husk.

[3] K. Saravanakumar, Harini Subramanian, V. Arumugam, H. N. Dhakal. Influence of milled glass fillers on the impact and compression after impact behavior of glass/epoxy composite laminates. *Polymer Testing* Volume 75, May 2019, Pages 133-141

Investigation into the effect of milled glass fiber fillers on GFRP with epoxy resin was carried out in this research study. With the optimum usage of the milled glass fiber filler on GFRP with epoxy resin, we can infer that the improvement in impact damage and residual CAI behaviors was evident. The glass filler-loaded samples resulted in a higher peak force than the baseline samples of GFRP. Thus, the improved properties of the glass fiber filler loaded GFRP are very good materials for the application of materials in aerospace and automotive industries as they possess good load-bearing applications.

[4] Kannivel Saravanakumar, Vellayaraj Arumugam, Rotte Souhith and Carlo Santulli. Influence of Milled Glass Fiber Fillers on Mode I & Mode II Interlaminar Fracture Toughness of Epoxy Resin for Fabrication of Glass/Epoxy Composites. *Fibers* 2020, 8(6), 36; <https://doi.org/10.3390/fib8060036>

Investigation of mode I and mode II interlaminar fracture toughness tests on GFRP were performed with various loadings of recycled milled glass fiber. The addition of milled glass fiber fillers (5 wt.%) with GFRP along with epoxy resin resulted in significant improvement in the interlaminar fracture toughness without affecting the flexural properties. Fractured surfaces analyzed using scanning electron microscopy (SEM) revealed several mechanisms, such as crack deflection, individual debonding, and filler/matrix interlocking, all contributing in various ways to improve fracture toughness.

[5] Manickam Ramesh, Lakshmi Narasimhan Rajeshkumar, Nagarajan Srinivasan, Damodaran Vasanth Kumar, and Devarajan Balaji. Influence of filler material on properties of fiber reinforced polymer composites: A review. *E-Polymers* 2022; 2:898–916. <https://doi.org/10.1515/epoly-2022-0080>

This paper briefly reviews the influence of filler material on the properties of FRP composites. In many cases, the addition of fillers with FRP composites resulted in obtaining higher mechanical and thermal properties. Filler material increases the adhesion between fiber and matrix and thus enhances water resistance. The filler addition increases the sound absorption coefficient of the FRP composites due to the porosity nature of the filler. Such filler reinforced composites find their applications in many areas requiring

electrical conductivity, dielectric medium, and in electrical and electronics applications due to the formation of dense percolation networks.

[6] A. Włodarczyk-Fligier, M. Polok-Rubinić, B. Chmielnicki. Polypropylene-Matrix Polymer Composites with Natural Filler. *Arch. Metall. Mater.* 66 (2021), 1, 313- 319. DOI: 10.24425/amm.2021.134789

Investigation into the effect of natural filler on polypropylene matrix polymer composites was carried out. The filler material used in this research study is walnut shell flour filler with various concentrations. A small effect on the filler fraction size was studied and observed. The low density of the material depends in particular on the material porosity. The composite material was characterized by low density, which increased with the rising filler content. The composites produced with filler are characterized by an increase in hardness and stiffness along with the increase in the filler content in the polypropylene matrix and a decrease in tensile strength was observed.

[7] Mauro Giorcelli, Aamer Khan, Nicola M. Pugno, Carlo Rosso, Alberto Tagliaferro. Biochar is a cheap and environmentally friendly filler able to improve polymer mechanical properties. *Biomass and Bioenergy* Volume 120, January 2019, Pages 219-223.

This research study reports the use of biochar derived from the maple tree as a filler material in epoxy resin matrix composites. The stiffness of the matrix was enhanced by the addition of small amounts of Biochar. Higher filler contents led to lower enhancement of the stiffness. The biochar filler addition affects the composite behavior transforming the blank epoxy from brittle to ductile composite. The addition of filler enhanced the young modulus and resilience. 1wt% addition led to a small enhancement of tensile toughness. From the study, we can infer that the addition of an optimum amount of biochar filler material influences the mechanical properties of the composite laminates.

[8] Halimatuddahlia Nasution, Hamidah Harahap, Rima Riani, Askalani Iqbal Pelawi. The Effect of Filler Particle Size on the Mechanical Properties of Waste Styrofoam Filled Sawdust Composite. *International Journal of Science and Engineering Investigations* vol. 7, issue 72, January 2018 ISSN: 2251-8843

Investigation into the effect of filler particle size on the mechanical properties of waste styrofoam-filled sawdust composite was carried out. The composites contained wt.% of 70 and 30 of Styrofoam and sawdust. The compatibilizer used was maleic anhydride. Results concluded that the incorporation of 150 microns has increased the mechanical properties of the composite such as tensile strength (33 MPa), flexural strength (15.4 MPa), and impact strength (300 J/cm²). The scanning electron microscopy (SEM) images of the 150-micron composite sample showed good distribution and a reduced amount of the voids present in the composite.

[9] Sunnatilla Aliev, Elmurod Egamberdiev, Sadriddin Turabdjano, Shokhzodbek Rashidov and Asror Juraev. Role of fillers in the production of wood-polymer composites. *E3S Web of Conferences* 434, 02030 (2023) ICECAE <https://doi.org/10.1051/e3sconf/202343402030>

Investigation of the effect of various properties by incorporating the filler with wood polymer composites (WPC). The resulting physical and mechanical properties are much greater than expected. The possibility of using WPC with fillers in outdoor construction work was confirmed with

the properties of water absorption and swelling composition. The filler incorporated WPC materials have a sufficiently high resistance to climatic factors.

[10] Erna Frida, Nurdin Bukit, Ferry Rahmat Astianta Bukit, Bunga Fisikanta Bukit. Effect of Hybrid Filler Oil Palm Boiler Ash – Bentonite on Thermal Characteristics of Natural Rubber Compounds. *Ecological Engineering & Environmental Technology* 2023, 24(2), 205–213 <https://doi.org/10.12912/27197050/156961>

Investigation on the thermal characteristics of natural rubber compounds with the addition of hybrid filler that is the oil palm boiler ash bentonite. The mechanical properties of the natural rubber compounds increase significantly with the addition of the hybrid filler. From the study, it is inferred that there is excellent interaction between the natural rubber compounds and hybrid filler material system and hence proved that the material is semicrystalline so that it can be processed.

[11] Oghenerukevw Prosper, Hilary Uguru. Effect of Fillers Loading on the Mechanical Properties of Hardwood Sawdust/Oil Bean Shell Reinforced Epoxy Hybrid Composites. 2018 IJSRSET | Volume 4 | Issue 8 | Print ISSN: 2395-1990 | Online ISSN: 2394-4099

This research study aims to prove that HSD, OBPS, and epoxy would be a substitute for Wood-based material composites in many industrial applications. The addition of natural fillers to epoxy matrix material improved the mechanical properties of the composite laminate (up to 50%), but after further increment in the weight of fillers led to a decrease in the mechanical properties. From the study, it is inferred that the composite material's mechanical properties are completely influenced by the filler loading and matrix adhesion.

[12] Sudeep Deshpande, T Rangaswamy. Effect of Fillers on E-Glass/Jute Fiber Reinforced Epoxy Composites. *Int. Journal of Engineering Research and Applications* ISSN: 2248-9622, Vol. 4, Issue 8 (Version 5), August 2014, pp.118-123

Investigation on the effect of mechanical properties of fiber-reinforced epoxy composite with the addition of varying concentrations of bone and coconut shell powders was carried out. The maximum impact strength was observed in the composite filled with 15% volume bone powder. The maximum ultimate tensile strength was observed in a composite filled with 10% volume coconut shell powder. Thus, it is inferred that the filler addition influences the mechanical properties of the fiber-reinforced composites.

[13] Gogu Venkateswarlu, Ravirala Sharada, and Mamidi Bhagvanth Rao. Effect of fillers on mechanical properties of PTFE-based composites. *Scholars Research Library Archives of Applied Science Research*, 2015, 7 (7):48-58

This research study focuses on the incorporation of fillers into the mechanical properties of polytetrafluoroethylene (PTFE). The different fillers that were used for the systematic study are glass, granite, graphite, garnet, alumina, antimony trisulphide, carbon, marble, mica, sand, bronze, wollastonite, porcelain, china clay, and tixolox – 25. Results indicated that the highest hardness value-based composites were found to be 15,20 and 25% in the case of garnet-filled PTFE, 50% in the case of marble-filled PTFE and 40% in porcelain-filled PTFE, 5% bronze-filled PTFE shows highest tensile strength and % elongation values. Some fillers failed to be incorporated as a

filler due to various reasons such as failure in some experimental tests.

[14] Sanjay Kumar M Sajjan, Vittal Kumar A Bongale, Atith D, B Yogesha. Study on the Mechanical Properties of Natural Fiber Reinforced Hybrid Composites with Natural Rubber as a Filler. *International Journal for Research in Engineering Application & Management (IJREAM)* ISSN: 2454-9150 Vol-06, Issue-09, DEC 2020.

Investigation on the effects of mechanical properties on the natural fiber reinforced hybrid composites with natural rubber as a filler material. The composites were fabricated by vacuum bagging technique. The tensile properties of ramie sisal composites remain the same despite the addition of filler. The tensile strength of the basalt-based composites was influenced by filler addition. The addition of natural rubber fillers enhanced the flexural properties of ramie-basalt composites. The impact properties are not influenced by the rubber composition.

[15] Stanley Jonathan M, Sharan Kumar L, Sudarshan D. S, Sharath Kumar M, Dr. Yogesha. K. K, Sandesh S Nayak. Effect of Silicon Carbide Fillers on the Mechanical Properties of Glass Fibre Reinforced Epoxy Polymer Composite. *International Research Journal of Engineering and Technology (IRJET)* Volume: 08 Issue: 07 | July 2021.

Investigation on the effect of mechanical properties of GFRP with silicon carbide as micro and nanofiller. The composites were fabricated by the hand layup method. The tensile strength, hardness, and flexural strength of nano-filled composites are found to be higher than micro SiC-filled composites. At 5 wt.% fillerloaded nano SiC-filled composites performed better as compared to the micro SiC-filled composites.

[16] Saravanakumar Kannivel, Harini Subramanian, Vellayaraj Arumugam, and Hom N. Dhakal. Low-Velocity Impact Induced Damage Evaluation and Its Influence on the Residual Flexural Behavior of Glass/Epoxy Laminates Hybridized with Glass Fillers. *Journal of Composites Science*. July 2020. 4(3): 99

This research work investigates experimentally the low-velocity impact-induced damage behavior and its influence on the residual flexural response of glass/epoxy composites improved with milled glass fillers. The low velocity impact damage employing varying impact velocities (3 m/s, 3.5 m/s, and 4 m/s) was induced on the baseline and filler-loaded samples with different fiber orientations. The residual performance and their damage modes were characterized using post-impact flexural (FAI) test and acoustic emission (AE) monitoring. In all fiber orientations, the filler-modified glass/epoxy samples showed improved impact strength and stiffness properties. A substantial improvement in impact damage tolerance, especially for samples impacted at 3.5 m/s and 4 m/s was observed. The presence of filler at the interlaminar zone contributed to improved energy dissipation through filler debonding and pull-out. This further contributed to arresting the crack growth, showing reduced damaged area. The inclusion of milled fibers on glass/epoxy laminates enhanced the impact of toughness and residual flexural behavior.

[17] M. Polok-Rubiniec, A. Włodarczyk-Fligier. Polypropylene matrix composite with charcoal filler. *JAMME* Volume 103 Issue 2 December 2020

Incorporation of charcoal powder as filler to investigate the thermal, electrical, and mechanical properties of polymer

composites. The samples were made by injection molding. After the experimental study and analysis, it is inferred that charcoal powder can be used successfully as a filler material for the polymer-based matrix to improve the mechanical properties of the composites. With an increase in the volume fraction of the filler in the matrix, the material's hardness increases significantly. The addition of filler into the matrix, increased electrostatic properties and worsened the electrical insulating properties.

[18] İlyas Kartal, Hilal Selimoğlu. Usability of Pine Sawdust and Calcite Together as Filler in Polyester Composites. *IJCESEN*. Vol. 9-No.3 (2023) pp. 267-273

This research study involves the investigation of polyester composites with polyester resin as matrix material and the fillers used are calcite and pine wood sawdust. Hence the usability of both natural and synthetic filler was investigated. Study from the tensile test, a partial decrease was observed as the sawdust filler increased, while this decrease was less in the case of calcite. No obvious change in impact properties was observed. The hardness results increased with the addition of both sawdust and calcite. It was understood from the SEM images that the fillers were homogeneously mixed in the structure. Finally, it is determined that the sawdust and calcite filler could be used together as fillers for material applications for large load bearing capacities.

From the literature review, it is clear that the influence of mechanical properties of the composite material with the addition of fillers (natural and synthetic fiber milled). The addition of optimum composition of fillers enhances the mechanical properties of composite materials. To satisfy the current trends of a wholesome material, the addition of fillers with matrix is considered to be a better option. Thus, the produced composite materials and structures are better suited for the application of aerospace and automotive industries.

3. EXPERIMENTAL PROCEDURE

3.1 Fillers and Chemicals Used

3.1.1 Basalt Filler



Figure 2: Basalt Uni-Directional Fibre (left), Powdered Basalt Filler (right)

Milled fibers are a short form of Basalt fibers, typically approximately 100µm in length, used as a reinforcing material in the composites industry. Milled fillers manufactured from recycled fibers are used in a wide range of applications when there is a need for improving mechanical properties like tensile strength and modulus. Basalt fibers can be applied in a wide range of application areas, i.e. thermal and acoustic insulation, pipelines, beams, fabrics, structural synthetic

materials, various car parts, reinforced concrete, insulating synthetic material, or friction material to name a few. Basalt is a natural quality raw material, which is not harmful to the environment. In contrast to many conventionally used fibers, basalt does not produce any toxic emissions during production and processing.

3.1.2 Areca Nut Filler

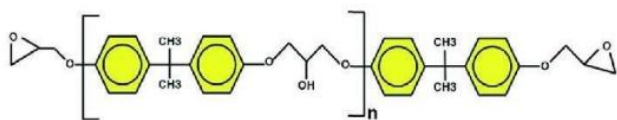
The husk fiber of the Areca nut is used as a lightweight, economically reinforcing material in industries such as construction, vehicle manufacturing, and aircraft manufacturing. The husk fiber is also used in the preparation of hard boards, paper boards, cushions, and non-woven fabrics. Milled Arecanut fibers are used as fillers in composite laminates to check their effect on the mechanical properties of composites such as Flexural properties.



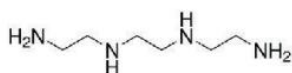
Figure 3: Areca Nut Filler

3.1.3 Epoxy and Hardener

Epoxy resin Araldite LY556 is extensively used as a reinforcing material due to its medium viscosity and chemical resistivity. The property of this resin can be easily modified within wide limits with the help of fillers and hardeners. The composition of this resin is based on Bisphenol-A which makes it suitable for high-performance FRP composite applications such as pultrusion, pressure molding, filament winding, and so on. This resin is known for its exceptional mechanical, good fiber impregnation, and thermal and dynamic properties. Also, epoxy resin LY556 has a low tendency to crystallize and hence it is preferred for aircraft and aerospace adhesives. Hardener Aradur HY951 is a low viscosity, unfilled epoxy casting resin system hardener, curing at room temperature with high filler addition possibility. The salient properties of this hardener include good mechanical strength, good resistance to atmospheric and chemical dehydration, and excellent electrical properties. Mixing an epoxy resin and a hardener starts a chemical reaction that produces heat- an exothermic reaction. It is claimed that after curing the bond is impervious to boiling water and all common organic solvents.



(a) Epoxy Resin (LY556)



(b) Epoxy Hardener - Araldite (HY951)

Figure 4: Chemical Composition of Epoxy Resin and Hardener

3.2 Ball Milling of Fibres

A ball mill is a type of grinder, that is a cylindrical device used in grinding (or mixing) materials like ores, chemicals, ceramic raw materials, and paints. Ball mills rotate around a horizontal axis, partially filled with the material to be ground plus the grinding medium. It works on the principle of impact and attrition: size reduction is done by impact as the balls drop from near the top of the shell. A ball mill consists of a hollow cylindrical shell rotating about its axis. The axis of the shell may be either horizontal or at a small angle to the horizontal. It is partially filled with balls. The grinding media are the balls, which may be made of steel (chrome steel), stainless steel, ceramic, or rubber, depending on the requirements.



Figure 5: Planetary Ball Mill Setup

Here, for our project purpose, we use a planetary ball mill, to grind the fibres into fine powders. The fiber is first cut into small pieces, and ground in the home appliance before putting it into the ball milling vile, for efficient milling.



Figure 6: Home Blended Basalt Fibres and Steel Balls

From literature surveys, the duration of grinding, ball to fibers ratio to be used, and Speed of rotation of the jars are found, which are as follows:

| | |
|-----------------------------|----------------|
| Fibres to balls wt. ratio : | 1:10 |
| Weight of fibre per run: | 20g |
| Weight of Steel Balls: | 200g |
| Ball Milling speed: | 732 rpm |
| Ball Milling Duration: | 4hrs |

Hence, the milling was done with the above conditions, to get the desired powder with a size in the range of micrometers, which can then be used as fillers.



Figure 7: Milled Basalt Fibre Filler

3.3 Fabrication of Epoxy Laminates

A silicone mold is created to hold the matrix and filler material mixture as part of the preparation for the specific laminate. This mold enables the simultaneous curing of ten samples. Using previously prepared composite samples with identical dimensions, the mold's impressions are created. For static flexural testing, the sample is estimated to be 150 mm x 25 mm x 4.5mm in size. The process of creating the test specimen starts once this mold is prepared. The epoxy resin LY 556 and the hardener HY 951 are mixed in a 10:1 ratio to create the base sample. First, the virgin epoxy sample is made without any filler added to it for comparison. Further in a similar fashion, the epoxy is added with fillers in weight fractions of 0.5%, 1%, 1.5%, 2%, 2.5%, and 3% respectively. In each weight percentage, five samples have been fabricated and tested for more accurate results. So, a total of 35 samples have been made with different weight percentages of milled basalt fillers. The milled Basalt fibers are combined with the epoxy resin using a magnetic stirrer. Using a magnetic stirrer, the epoxy resin and milled filler mixture are blended for 2 hours at 60 60-degree temperature. The magnetic stirrer ensures that the fibers and epoxy resin are mixed uniformly, creating uniform dispersion without any air bubbles or voids.



Figure 8: Magnetic Stirrer

The stirring in a magnetic stirrer is followed by placing the mixture in a sonicator for ultrasonic dispersion. The sonicator is simple to use and adaptable since it effectively disperses the particles in the epoxy. With the aid of the shock waves generated by cavitation in the ultrasonic mixture, it breaks down the surrounding covalent bonds. The epoxy resin

and milled fiber mixture are stirred for 32 minutes using this magnetic stirrer.



Figure 9: Sonicator

The mixture is now allowed to cool for some time, and the hardener is added in the ratio of 1:10 hardener to mixture ratio. The mixture is now stirred using a stick, manually, and carefully so that no air bubbles are formed, and until the hardener disperses well into the mixture. This mixture is then poured into silicone molds where they are allowed to cure for 24 hours.



Figure 10: Mixture Poured into Silicone Mould for Curing

Before the mixture is cured fully, it is taken from the mold within 24 hours, to perform post curing process, in which the samples are left in the temperature chamber for two hours at 90°C. This post-curing in the temperature chamber ensures the breakage of the O-H bond of epoxy, and the necessary chemical bonding to take place between the epoxy and filler materials.



Figure 11: Temperature Chamber

The milled basalt fillers utilized have weight percentages of 0.5%, 1%, 1.5%, 2%, 2.5%, and 3%, respectively. In the same manner, five samples in each weight percentage have been created and evaluated to ensure more precise findings. So, 35 samples in all have been created using various weight ratios of milled Basalt fillers. From the epoxy samples fabricated and tested, the weight percentages of samples obtained will finally be tested and optimal results have been obtained which are then used for the fabrication of composite samples, with Basalt fiber and epoxy resin as fiber and matrix materials respectively, where the optimal weight percentage of milled basalt filler is added to the epoxy resin.

| Composition of the sample | Epoxy samples | Total no. of samples |
|--|---------------|----------------------|
| Base sample without filler | 05 | 05 |
| Sample with 0.5% milled Basalt fillers | 05 | 30 |
| Sample with 1% milled Basalt fillers | 05 | |
| Sample with 1.5% milled Basalt fillers | 05 | |
| Sample with 2% milled Basalt fillers | 05 | |
| Sample with 2.5% milled Basalt fillers | 05 | |
| Sample with 3% milled Basalt fillers | 05 | |
| Total no of epoxy samples | | 35 |

Table 1: Quantity of Epoxy Samples Fabricated for Static Testing and their Filler Composition

3.4 Procedure for Static Testing

Pure epoxy, and 0.5%, 1%, 1.5%, 2%, 2.5%, and 3%, milled basalt fiber composition samples were created. The samples are tested using a Universal Testing Machine (UTM). The table below lists the specifications of the Universal Testing Machine. The flexural properties of the samples have to be examined, hence a three-point bending test is performed.

| UNIVERSAL TESTING MACHINE Specifications | |
|--|------------|
| Force capacity | 100 kN |
| Minimum test speed | 0.1 mm/min |
| Maximum test speed | 500 mm/min |
| Crosshead return speed | 700 mm/min |

Table 2: Specifications of Universal Testing Machine (UTM)

With the loading device in the center, the sample should be positioned evenly on the UTM's supports. To create a span, the supports should be placed so that their distance from one another is greater than the length of the sample. To guarantee that the sample is appropriately aligned, the supports should be raised or lowered to the proper height and level. The loading device should be used to exert pressure on the sample's center after the UTM has been set to the proper load rate.



Figure 12: Virgin Epoxy Samples before Testing



Figure 13: Epoxy Samples with Milled Basalt Fillers after Testing

As the force is raised, the UTM should gauge and note the sample's load and displacement. Continue the test until the sample breaks or deforms. To determine the material's flexural strength and stiffness, the data gathered during the test should be analyzed. The yield strength, elastic modulus, and other material parameters can all be determined using the UTM software. The sample's concave side is compressed during this test, while its convex side is under tension.

4. RESULTS AND DISCUSSIONS

For the investigation of flexural properties, plain epoxy samples are compared to milled basalt filler concentrations of 0.5%, 1%, 1.5%, 2%, 2.5%, and 3%, weight fractions. The samples are examined for flexural characteristics using the Universal Testing machine (UTM).



Figure 14: Three-Point Flexural Test

The three-point bending method is applied for testing and load is exerted till the point of rupture. The results

obtained from the flexural test are tabulated, plotted, and discussed below.

4.1 Epoxy Samples (Static Testing)

It is very well known that cured pure epoxy is brittle i.e., it fractures when subjected to stress but has little tendency to deform before rupture. Furthermore, it has a poor capacity to resist the impact and vibration of loads. From the Force vs Position graph for milled fibers, it can be seen that the ultimate yield force gradually increases with the increase in milled fibers concentration.

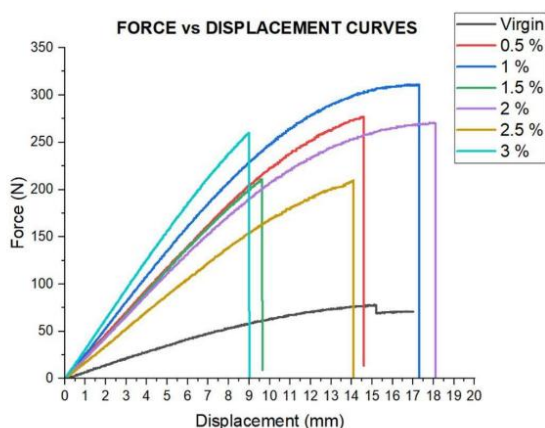


Figure 15: Load Vs Displacement Graph of Epoxy Samples with Basalt Fillers

Also, from the graphs, it can be noted that up to a particular weight concentration, the ultimate yield force increases with an increase in weight percentage. After a certain weight fraction of fillers in epoxy laminate, the ultimate yield force decreases with an increase in weight percentage. The percentage at which the maximum ultimate yield force is obtained is taken as the percentage of interest for which the flexural properties are analyzed. For samples with milled Basalt fibers, the maximum ultimate yield force is obtained for 1% weight percentage. Flexural strength, flexural toughness, and flexural modulus are the properties that are being analyzed. For this purpose, these values are being plotted against the weight percentage of milled fillers to get the required values.

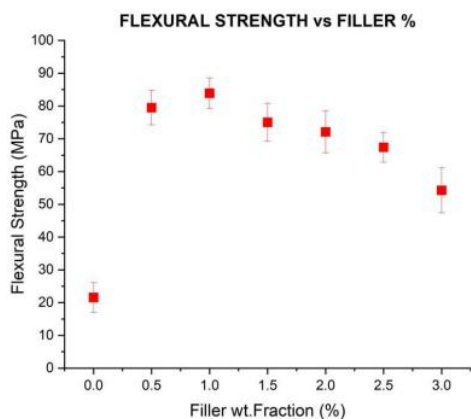


Figure 16: Flexural Strength Vs Weight Concentration Graph for Epoxy Samples with Milled Basalt Fillers

Flexural strength refers to the ability of a material to resist bending or deformation when subjected to an external

force or load. It measures the maximum stress a material can withstand before it breaks or fractures. For Epoxy samples with different concentrations of milled Basalt fillers, the maximum flexural strength is obtained for samples with 1% milled Basalt fillers which is 81.884 MPa.

$$\sigma = \frac{3FL}{2bd^2}$$

Where, σ = Flexural Strength (MPa)

F = Ultimate load (N)

L = Effective span of sample (m)

b, d = Breadth and Depth of the sample (m)

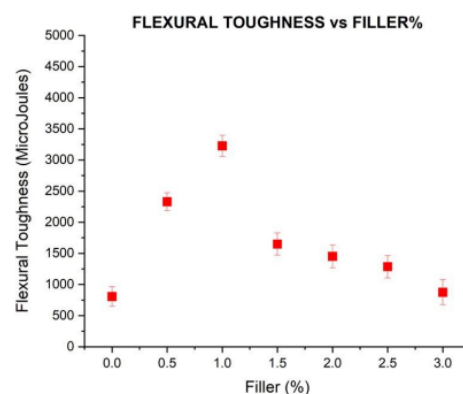


Figure 17: Flexural Toughness Vs Weight Concentration Graph for Epoxy Samples with Milled Basalt Fillers

Flexural toughness is the ability of the composite to absorb energy and resist fracture when subjected to bending loads. In this case, epoxy samples with 1% of milled Basalt fibers have a higher flexural toughness value of 3227.4106 MPa compared to Epoxy samples with other weight percentages. The area under the curves for the plot of each weight percentage depicts the energy absorbed to proceed to failure which is essentially the toughness of the material. From a primary analysis, it is noted that as the weight percentage of the milled fibers increases, the toughness also increases which can be visualized from the graph above.

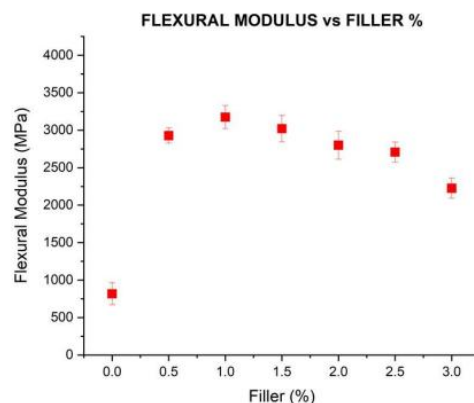


Figure 18: Flexural Modulus Vs Weight Concentration Graph for Epoxy Samples with Milled Basalt Fillers

Flexural modulus or bending modulus is defined as the ratio of stress to strain in flexural deformation, or the tendency for a material to resist bending. It is determined from the slope of a stress-strain curve produced by a flexural test. In the case of flexural modulus too, Epoxy samples with 1% of milled Basalt fillers have a higher flexural toughness value of 3175 MPa compared to Epoxy samples with other weight percentages of milled Basalt fillers. From the graphs above plotted, it is evident that all three flexural properties are higher for 1% weight percentage of milled Basalt fillers.

These properties are being compared with the base sample of epoxy resin without any milled fillers which is being tabulated below.

| Properties | Base Sample (MPa) | Sample with 1% milled Basalt fibers (MPa) | Percentage increase (%) |
|-----------------------|-------------------|---|-------------------------|
| Ultimate yield stress | 25.7 | 99.7 | 287.93 |
| Flexural Strength | 21.578 | 81.888 | 279.49 |
| Flexural Toughness | 807.31 | 3227.41 | 299.71 |
| Flexural Modulus | 817.187 | 3175 | 288.52 |

Table 3: Comparison of Properties of Base Epoxy Samples and Samples with 1% Milled Basalt Fibre Fillers

4.2 Basalt/Epoxy Samples (Static Testing)

Following the optimization of the weight percentage of milled Basalt fillers in epoxy resin to be used, we move ahead with manufacturing composite laminate with Basalt as fiber and epoxy as resin. A base sample without filler is being manufactured, followed by making 1% milled basalt filler incorporated sample. A hand layup process was used to make the laminate with proper precautions. 16 layers of Basalt UD fibre were cut each having dimensions of 200 x 200 mm. The resin-to-hardener ratio taken was 10:1. Following the layup process, the composite laminate was placed in a compression molding chamber to speed up the curing process. Compression molding was performed for 15 minutes at around 90 degrees Celsius.



Figure 19: Hand Lay Up of Basalt/Epoxy Composite Laminate

4 samples each were taken in both Base and filler incorporated Basalt/Epoxy composites, after cutting to proper ASTM standard dimensions., and tested until the failure point in the Universal Testing Machine.



Figure 20: Base Basalt/Epoxy Samples (Left); Basalt/Epoxy + Filler Samples (Right)

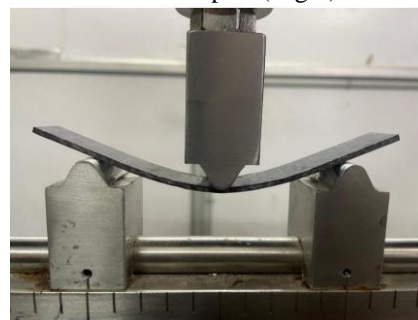


Figure 21: Three Point Bending Test being done in UTM

The load versus displacement graphs are plotted for Basalt fiber composite samples with 1% milled Basalt fillers and also for composite samples without any fillers.

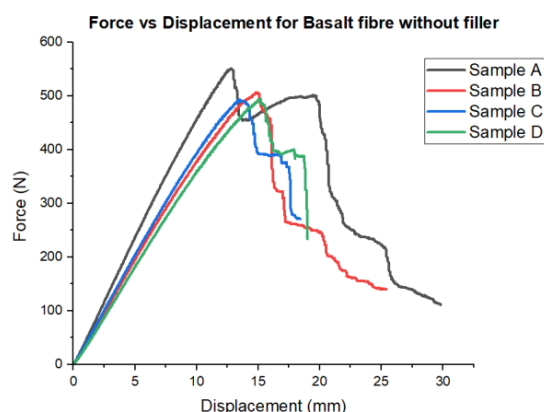


Figure 22: Load Vs Displacement Graph for Basalt Fiber Composite Sample without Fillers (Base Samples)

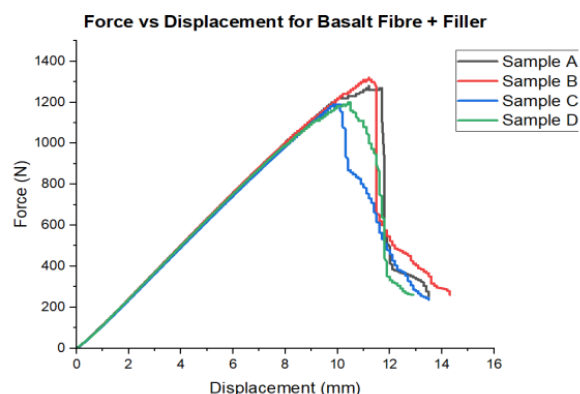


Figure 23: Load Vs Displacement Graph for Basalt Fiber Composite Sample with Milled Basalt Fillers

With the above load versus displacement graphs, it is possible to compare and analyze the load-carrying capacity of Basalt/Epoxy composites with and without filler.

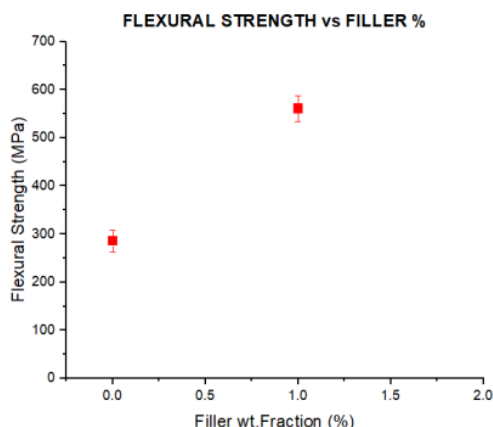


Figure 24: Comparison of Flexural Strength Vs Filler Weight Percentage Graph for Basalt/Epoxy Composite Samples

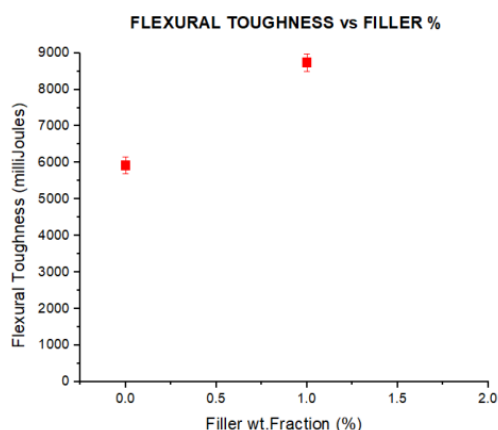


Figure 25: Comparison of Flexural Toughness Vs Filler Weight Percentage Graph for Basalt/Epoxy Composite Samples

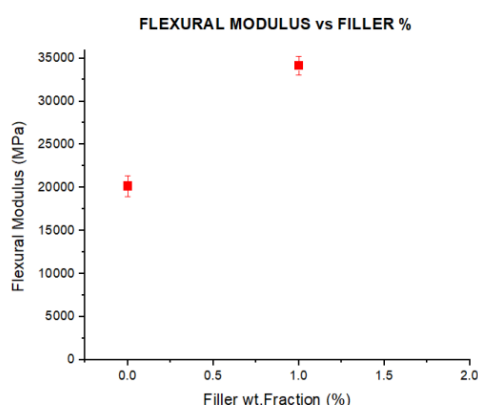


Figure 26: Comparison of Flexural Modulus Vs Filler Weight Percentage Graph for Basalt/Epoxy Composite Samples

The three aforementioned graphs demonstrate how the flexural properties depend on the filler weight percentage. It is evident that when compared to the base composite sample, the filled incorporated Basalt/Epoxy composite sample with 1% milled fillers exhibits higher values for flexural properties. Furthermore, the load-carrying capacity improves.

| Properties | Base sample (MPa) | Sample with 1% milled Basalt fibers (MPa) | % increase of property from base sample |
|-------------------------|-------------------|---|---|
| Ultimate Load (N) | 507.535 | 1246.712 | 145.64% |
| Flexural strength | 285.488 | 561.0206 | 96.51% |
| Flexural Toughness (mJ) | 5919.39 | 8738.64 | 47.67% |
| Flexural Modulus | 20,175 | 34,125 | 69.14% |

Table 4: Comparison of Properties of Base Basalt/Epoxy Composite Sample and Sample with Milled Fibres

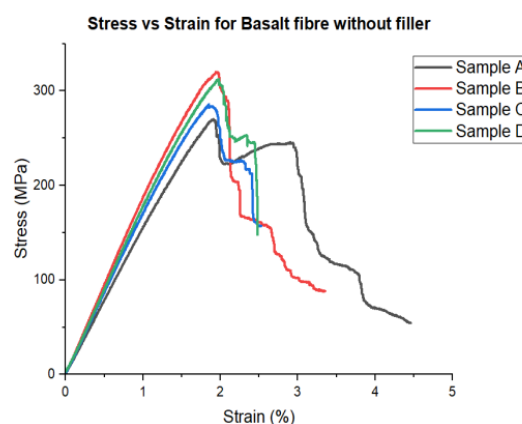


Figure 27: Stress Vs Strain Graph for Basalt Fiber Composite without Filler

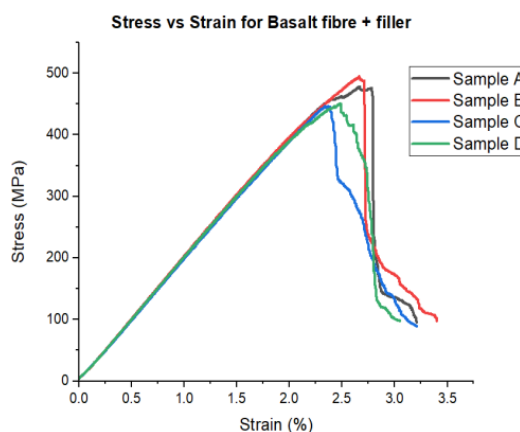


Figure 28: Stress Vs Strain Graph for Basalt Fiber Composite with Filler

4.3 Simulation in ANSYS – Basalt/Epoxy Laminate

The structural simulation is done for the Basalt/Epoxy composite sample without fillers, and with 1% milled Basalt fibers. To assess the stress distributions, the equivalent stress contours have been displayed. The deformation contour obtained from the ANSYS simulation of the three-point bending test provides crucial information about the structural response of the beam specimen under the applied load. By analyzing the deformation contour, it is possible to identify areas of significant deflection and

deformation. In this beam specimen, it is noted that the deformation is maximum at the loading point which is at the center of the beam. The CAD model was designed by a design modeler in ANSYS. The dimension of laminate is (150 x 25 x 4.5) mm according to ASTM Standards.

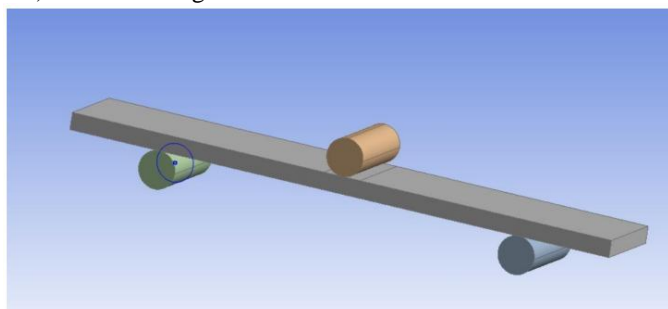


Figure 29: Composite Model Designed in Design Modeller in ANSYS

The meshing was done separately for the laminate and the support rollers. Additionally, face meshing was done for the 6 faces of the rollers. The element size for the mesh given was: 2mm.

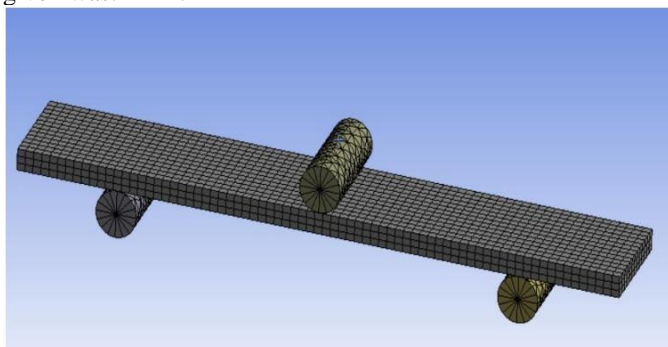


Figure 30: Meshing of Basalt/Epoxy Model

The stress contour obtained from the ANSYS simulation of the three-point bending test provides valuable insights into the behavior of the beam specimen under loading conditions. By analyzing the stress distribution, it is possible to identify regions of high-stress concentrations, such as near the loading points or at the supports. These regions indicate potential areas of weakness or failure.

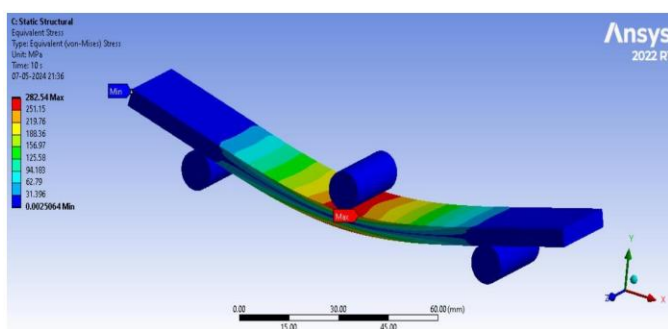


Figure 31: Equivalent Stress Contour of Basalt/Epoxy Composite without Fillers

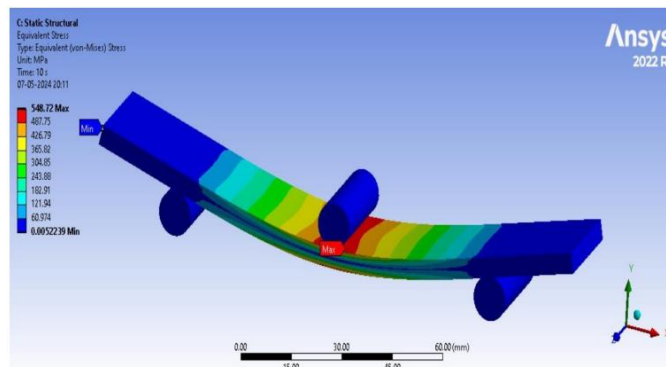


Figure 32: Equivalent Stress Contour of Basalt/Epoxy Composite with 1% Milled Basalt Fillers

| SAMPLE | SIMULATION VALUE OF ULTIMATE STRESS (in Mpa) | EXPERIMENTAL VALUE OF ULTIMATE STRESS (in Mpa) |
|------------------------|---|--|
| Base sample | 282.54 | 285.488 |
| 1% filler added sample | 548.72 | 561.0206 |

Table 5: Comparison of Ultimate Stress Values from Experiment and Simulation of Basalt/Epoxy

From the above table, it is evident that simulation and experimental values match each other to a greater extent, hence providing a scope, that the approach goes in the right manner, to study the effect of milled filler on the flexural properties of natural fiber composites.

4.4 ArecaNut/Epoxy Samples (Static Testing)

Following the static testing of Basalt/Epoxy laminate with and without filler being added, we move ahead with manufacturing composite laminate with Arecanut as fiber and epoxy as resin. A base sample without filler is being manufactured, followed by making 1% milled basalt filler incorporated Arecanut/Epoxy sample. A hand layup process was used to make the laminate with proper precautions. 4 layers of Arecanut UD fibre were cut each having dimensions of 200 x 200 mm. The resin-to-hardener ratio taken was 10:1. Following the layup process, the composite laminate was placed in a compression molding chamber to speed up the curing process. Compression molding was performed for 15 minutes at around 90 degrees Celsius.



Figure 33: Hand Lay Up of Areca Nut/Epoxy Composite Laminate



Figure 34: Compression Moulding in the Moulding Chamber



Figure 35: Areca Nut/Epoxy Sample Post Compression Moulding

4 samples each were taken in both Base and filler incorporated Arecanut/Epoxy composites, after cutting to proper ASTM standard dimensions., and tested until the failure point in a Universal Testing Machine.



Figure 36: Base ArecaNut/Epoxy Samples

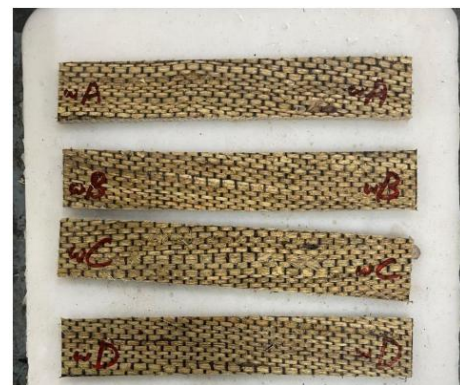


Figure 37: ArecaNut/Epoxy Samples added with Milled Basalt Filler

The load versus displacement graphs are plotted for Arecanut fiber composite samples with 1% milled Basalt fillers and also for composite samples without any fillers.

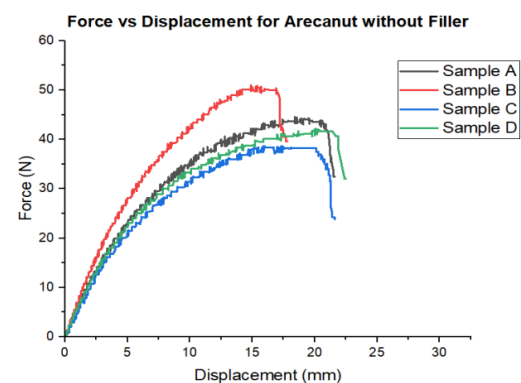


Figure 38: Load Vs Displacement Graph for ArecaNut Fiber Composite Sample without Fillers (Base Samples)

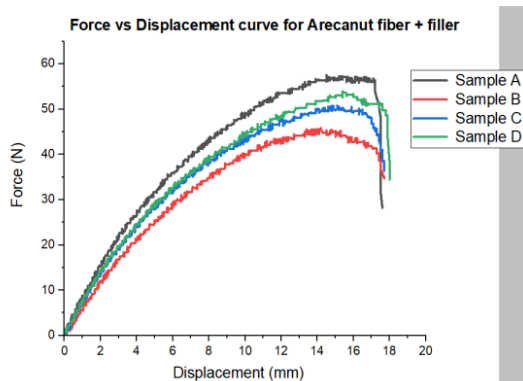


Figure 39: Load Vs Displacement Graph for ArecaNut Fiber Composite Sample with Milled Basalt Fillers

With the above load versus displacement graphs, it is possible to compare and analyze the load-carrying capacity of Arecanut/Epoxy composites with and without filler.

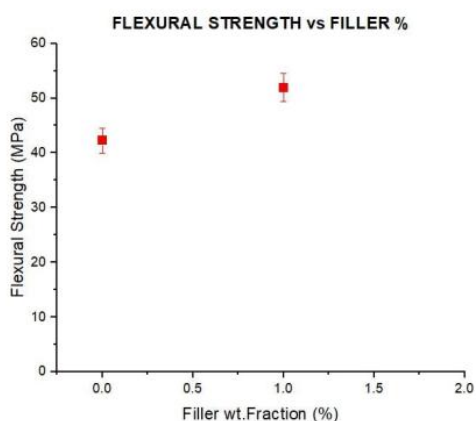


Figure 40: Comparison of Flexural Strength Vs Filler Weight Percentage Graph for ArecaNut/Epoxy Composite Samples

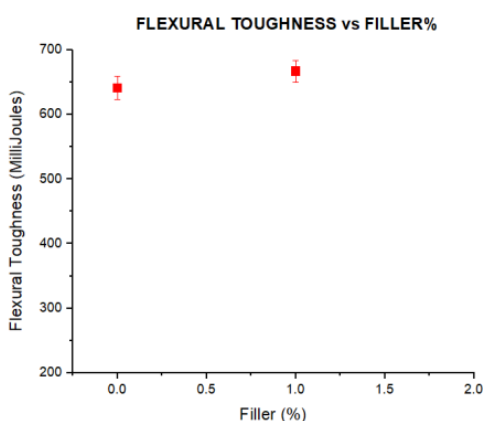


Figure 41: Comparison of Flexural Toughness Vs Filler Weight Percentage Graph for ArecaNut/Epoxy Composite Samples

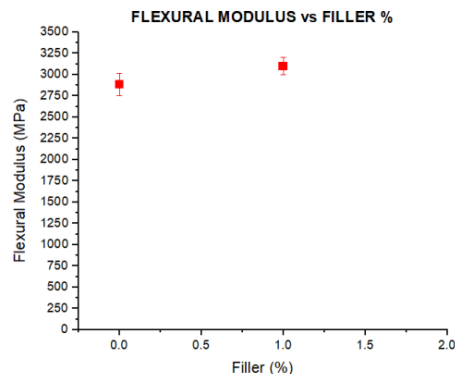


Figure 42: Comparison of Flexural Modulus Vs Filler Weight Percentage Graph for ArecaNut/Epoxy Composite Samples

The three aforementioned graphs demonstrate how the flexural properties depend on the filler weight percentage. It is evident that when compared to the base composite sample, the filled incorporated Arecanut/Epoxy composite sample with 1% milled fillers exhibits higher values for flexural properties. Furthermore, the load-carrying capacity improves.

| Properties | Base Arecanut/Epoxy sample (MPa) | Sample with 1% milled Basalt fillers (MPa) | % increase of property from base sample |
|-------------------------|----------------------------------|--|---|
| Ultimate Load (N) | 46.445 | 54.056 | 16.38% |
| Flexural strength | 42.263 | 51.894 | 22.78% |
| Flexural Toughness (mJ) | 640.688 | 666.387 | 4.01% |
| Flexural Modulus | 2885 | 3100 | 7.45% |

Table 6: Comparison of Properties of Base ArecaNut/Epoxy Composite Sample and Sample with Milled Fibers

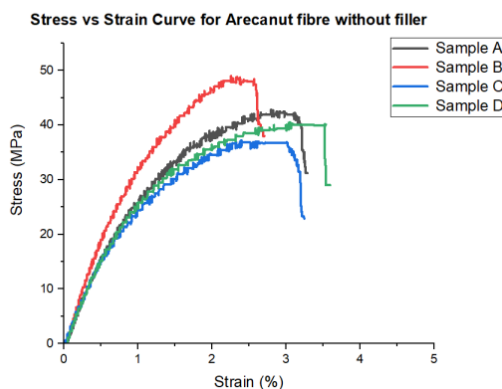


Figure 43: Stress Vs Strain Graph for ArecaNut Fiber Composite without Filler

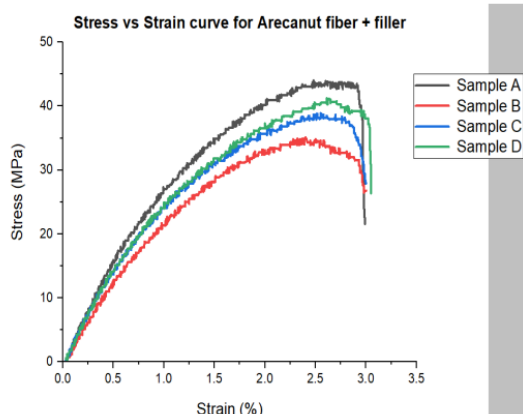


Figure 44: Stress Vs Strain Graph for ArecaNut Fiber Composite with Filler

4.5 Simulation – ArecaNut/Epoxy Laminate

The structural simulation is done for the Arecanut/Epoxy composite sample without fillers, and with 1% milled Basalt fibers. To assess the stress distributions, the equivalent stress contours have been displayed. The deformation contour obtained from the ANSYS simulation of the three-point bending test provides crucial information about the structural response of the beam specimen under the applied load. By analyzing the deformation contour, it is possible to identify areas of significant deflection and deformation. In this beam specimen, it is noted that the deformation is maximum at the loading point which is at the center of the beam. The CAD model was designed by a design modeler in ANSYS. The dimension of laminate is (150 x 25 x 4.5) mm according to ASTM Standards.

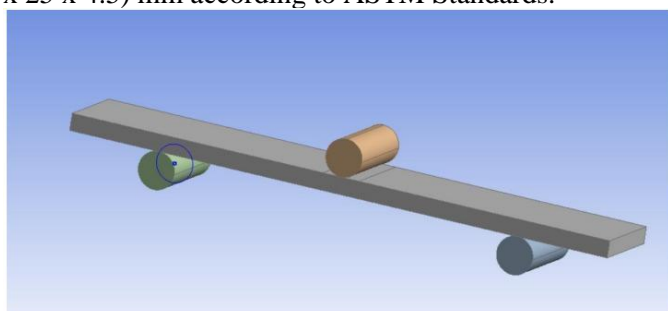


Figure 45: Design of ArecaNut/Epoxy Model

The meshing was done separately for the laminate and the support rollers. Additionally, face meshing was done for the 6 faces of the rollers. The element size for the mesh given was: 2mm.

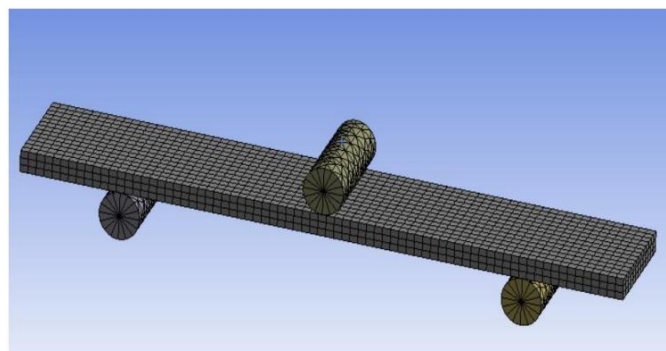


Figure 46: Meshing of ArecaNut/Epoxy Model

The stress contour obtained from the ANSYS simulation of the three-point bending test provides valuable insights into the behavior of the beam specimen under loading conditions. By analyzing the stress distribution, it is possible to identify regions of high-stress concentrations, such as near the loading points or at the supports. These regions indicate potential areas of weakness or failure.

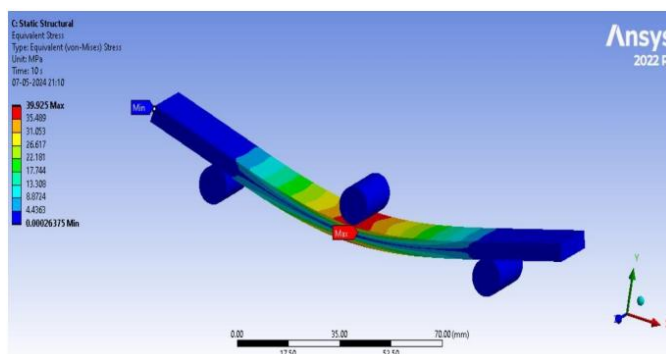


Figure 47: Equivalent Stress Contour of ArecaNut/Epoxy Composite without Fillers

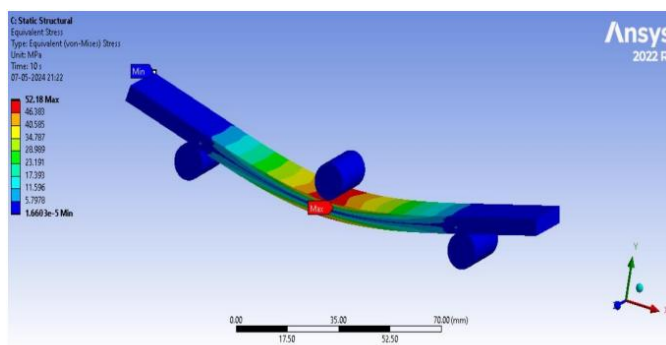


Figure 48: Equivalent Stress Contour of ArecaNut/Epoxy Composite with 1% Milled Basalt Fillers

| SAMPLE | SIMULATION VALUE OF ULTIMATE STRESS (in Mpa) | EXPERIMENTAL VALUE OF ULTIMATE STRESS (in Mpa) |
|------------------------|---|--|
| Base sample | 39.925 | 42.263 |
| 1% filler added sample | 52.18 | 51.894 |

Table 7: Comparison of Ultimate Stress Values from Experiment and Simulation of ArecaNut/Epoxy

From the above table, it is evident that simulation and experimental values match each other to a greater extent, hence providing a scope, that the approach goes in the right manner, to study the effect of milled filler on the flexural properties of natural fiber composites.

5. CONCLUSIONS

5.1 Resin Study (Optimization of Filler%)

The resin study of the samples with milled basalt fillers is analyzed for further fabrication of the composite with the optimum weight percentage of the milled fillers showing the desired results. Using milled fibers as fillers shows promising results in terms of flexural properties as well as the load-carrying capacity of the resin samples. As we proceeded from 0.5 % filler to 3% filler incorporated epoxy samples, we observed that we got maximum flexural properties such as Flexural Strength, Flexural Toughness, and Flexural Modulus, at a 1% weight fraction of Basalt filler in epoxy sample. The properties increase because, the addition of filler enhances the fracture toughness behavior of the matrix, resulting in more efficient load transfer by arresting and diverting the crack. The fillers in the resin arrest crack propagation by preventing the expansion of matrix micro-cracking. Micro cracks forming in the matrix due to the load are better dissipated as the filler is dispersed equally in the matrix, the milled fibers tend to form bridges between the cracks and hold together the matrix increasing flexural properties. However, after 1% concentration, an increase in the concentration of the milled fibers causes a decrease in the ultimate yield stress. So consequently, a decrease in the flexural properties is also noted for an increase in the weight percentage after this optimum weight concentration. This happens due to agglomeration of the milled fibers taking place due to Vander Waals attraction between the molecules of the milled fibers, at higher weight percentages. Hence, we have used this ideal weight fraction of 1% milled Basalt filler in the composite laminates to be made with Basalt and Arecanut fibers and epoxy as resin, which has been done further, and necessary flexural testing has been carried out to determine their mechanical properties. These properties have been compared

with their respective base composite samples, which are not added with milled filler.

5.2 Basalt/Epoxy Composite – Static Testing

At the end of the static testing of both base and filler-incorporated samples, we found a significant enhancement of flexural properties such as Flexural strength, modulus, and toughness. Max. The ultimate force of 1246.712 N was observed for the Basalt/Epoxy sample with 1% Milled filler incorporated sample. Hence, the increase in Ultimate force value from that of the Base Composite (Basalt/Epoxy) sample is: 2.46 times. Max. Flex. A strength of 561.0206 MPa was observed for the Epoxy sample with 1% Milled filler incorporated sample. Hence, increase in Flex. The strength value from that of the Base Composite (Basalt/Epoxy) sample is: 1.96 times. Max. Flex. The toughness of 8.738 Joules was observed for the Epoxy sample with 1% Milled filler incorporated sample. Hence, increase in Flex. The toughness value from that of the Base Composite (Basalt/Epoxy) sample is: 1.476 times. Max. Flex. A modulus of 34.125 MPa was observed for the 1% Filled filler incorporated sample. Hence, increase in Flex. The modulus value from that of the Base Composite (Basalt/Epoxy) sample is: 1.69 times. The increase in the flexural properties in the filler-loaded sample, compared to the base sample can be attributed to the fact that ball milling leads to roughening of the surface of the fiber, the rough surface of the fiber helps in better interfacial bonding with the matrix and also prevents pull-out of the fiber due to increased friction, hence leading to an improvement in properties. Moreover, the filler enhances the adhesion between the fiber and the matrix, reducing the scope of delamination. Transverse matrix cracking and fiber-matrix interface debonding are reduced by improving the interlaminar properties of brittle epoxy matrix by incorporation of fillers

5.3 ArecaNut/Epoxy Composite – Static Testing

Similarly, at the end of the static testing of both base and filler incorporated samples, of Arecanut/Epoxy composite, we have found an enhancement of flexural properties, but of lower significance when compared with that of Basalt/Epoxy laminate. Max. The ultimate force of 54.056 N was observed for 1% Milled Basalt filler incorporated sample. Hence, the % increase in Ultimate force value from that of the Base Composite (Arecanut/Epoxy) sample is: 16.38 %. Max. Flex. A strength of 51.894 MPa was observed for 1% Milled Basalt filler incorporated sample. Hence, increase in Flex. The strength value from that of the Base Composite (Arecanut/Epoxy) sample is: 22.78 %. Max. Flex. The toughness of 0.66 Joules was observed for the 1% Milled Basalt filler incorporated sample. Hence, % increase in Flex. The toughness value from that of the Base Composite (Arecanut/Epoxy) sample is: 4.01 %. Max. Flex. A modulus of 3100 MPa was observed for the 1% Milled Basalt filler incorporated sample. Hence, increase in Flex. The modulus value from that of the Base Composite (Arecanut/Epoxy) sample is: 7.45 %. The increase in flexural properties of the filler-loaded sample to that of the base sample can be

explained in a similar way as done for basalt/epoxy composites. However, here the % increase in properties is not as significant as compared with basalt/epoxy composites. This may be because, the milled filler is of basalt and the fiber material is areca nut here, so the adhesion between matrix and fiber might not be as strong as in the case of basalt/epoxy composite, where the filler and fiber both are of same material (Basalt). However, this conclusion is not based on any literature surveys.

| Flexural Properties | % Increment of properties of Filler + Basalt/Epoxy composite from Base sample | % Increment of properties of Filler + Arecanut/Epoxy composite from Base sample |
|-------------------------|---|---|
| Ultimate Load (N) | 145.64 % | 16.38 % |
| Flexural strength (MPa) | 96.51 % | 22.78 % |
| Flexural Toughness (mJ) | 47.62 % | 4.01 % |
| Flexural Modulus (MPa) | 69.14 % | 7.45 % |

Table 8: Comparison of properties enhancement in both Basalt and ArecaNut Samples

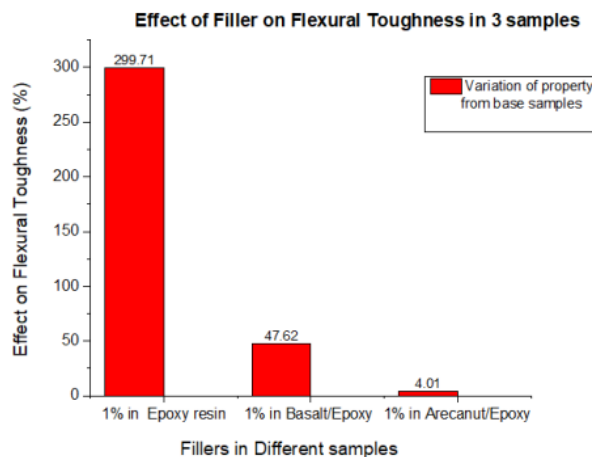


Figure 50: Effect of Filler on Flexural Toughness of Samples with Fillers in Comparison with their base samples

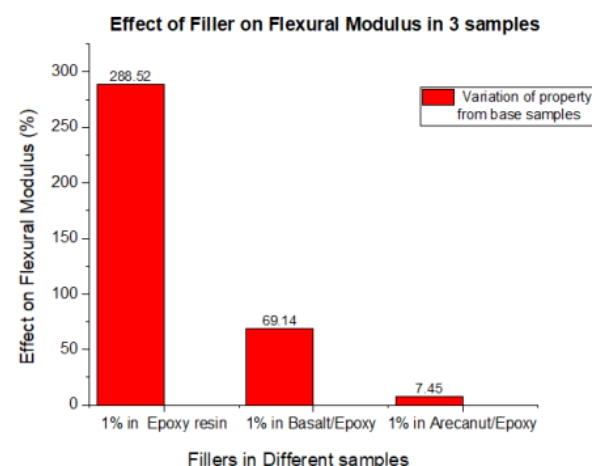


Figure 51: Effect of Filler on Flexural Modulus of Samples with Fillers in Comparison with their base samples

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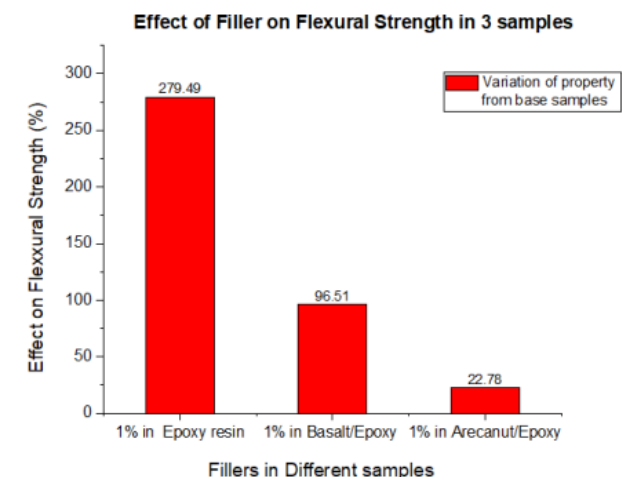


Figure 49: Effect of Filler on Flexural Strength of Samples with Fillers in Comparison with their base samples

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