

# Design, Analysis & Fabrication of Drilling and Tapping Machine

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## Abstract :-

This paper presents the design and analysis of an automatic drilling and tapping machine aimed at enhancing efficiency and precision in machining operations. The study focuses on the conceptualization and development of a comprehensive machine model that integrates drilling and tapping functionalities within a single automated system. Key design parameters, including spindle speed, feed rate, tool dimensions, and material compatibility, are analyzed to ensure optimal performance and reliability. A detailed CAD model is developed, followed by structural and functional analysis to validate the machine's design.

The design data for the model includes specifications for the motor, spindle, and feed mechanisms, along with material properties and operational constraints. These data points were used to optimize the system's performance and ensure the machine's suitability for a wide range of machining tasks.

**Key Words :-** Drilling, Tapping, Design, Measurement , Automation

**1. Introduction:-** The topic "Design & fabrication of Drilling and Tapping Machine" is about creating a machine that can drill holes and cut threads (tapping) in one setup. The design process involves creating the machine's structure, including the spindle, base, and tool holders, ensuring they can handle the forces during drilling and tapping. Key design factors include material selection for durability, optimizing the geometry to reduce weight while maintaining strength, and ensuring smooth tool alignment for precision. Advanced CAD software is used for 3D modelling.

**1.1 Drilling Process:-** The drilling process is a systematic method used to create holes in materials by removing material using a rotating cutting tool. It involves stages such as selecting the appropriate drill bit, aligning the workpiece, and applying controlled force and speed to achieve precise and efficient results.

**1.2 Tapping Process:-** The tapping process is a machining operation used to create internal threads within a pre-drilled hole using a tool called a tap. It involves precise alignment of the tap with the hole, controlled rotation, and to ensure accurate threading and avoid damage to the tool or workpiece.

**2. Design of Components :-** The design data for an automatic drilling and tapping machine includes critical parameters such as spindle speed, feed rate, motor power, tool dimensions, and material specifications. These data points serve as the foundation for optimizing the machine's performance, ensuring precision, durability, and suitability for specific industrial applications.

**I. Motor:** It is a 3 Phase 0.5 H.P. Motor and runs at 720 rpm & is mounted on the bracket.

**II. Table:** The Table ( 90 MM X 130 MM ) is mounted on the column and is provided with 'T' bolts for clamping the

work directly on its face. The table is made as a rectangular in shape. It is made of Cast Iron.

**III. Base:** The Base is that part of the machine on which the vertical column is mounted. The Base is made of Cast Iron.

**IV. Column:** The column is the vertical member (500 mm X  $\varnothing$ 45mm) of the machine, which supports the table and the head containing all the driving mechanism.

**V. Cone Housing:** The cone housing is made up of mild steel. Initially a square bar of 80mm x 80mm of length 280mm is machined. A drill of 45mm is made on one side for a depth of 75mm. A cylindrical bar of dia 80mm and length 100mm is welded to the square bar at a distance of 64mm from the top.

**VI. Worm and worm gear :** It consist of Worm with 4 teeth and Worm gear with 30 teeth. Diameter of gear = 90mm , Diameter of worm = 50mm.

**VII. Table Housing:** The table housing is made up of mild steel. A collar of inner dia 45mm wnr outer 55mm is machined and it is cut on one side alone the axis and two flats are welded. The Table Housing slides over the Column of the Machine.

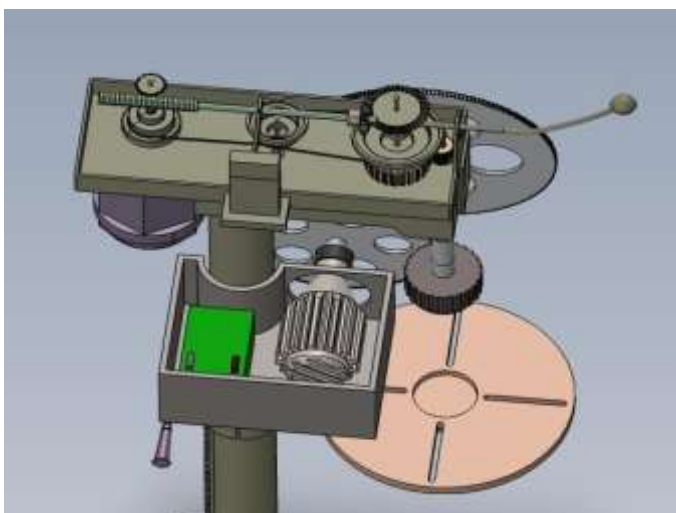
**VIII. Main Vertical Spindle:** The Spindle is mounted vertically (220 mm X  $\varnothing$ 22mm) held between bushes and its carries two M. S. Cones one end of the spindle is attached to the drill Chuck to hold the tool. The spindle rotates in the either direction according to the engagement of Cones.

**IX. Drill Chuck:** The self-cantering 3 jaw chuck is particularly adapted for holding tools having straight shanks. The chuck is tightened and loosened by rotating a bevel key meshed with bevel teeth of the sleeve.

**X. Bolts & Nuts:** It is used to fix the motor with Base, to fix the column support to the base. The Grub screw to fasten the M.S. Cones to the vertical Spindle.

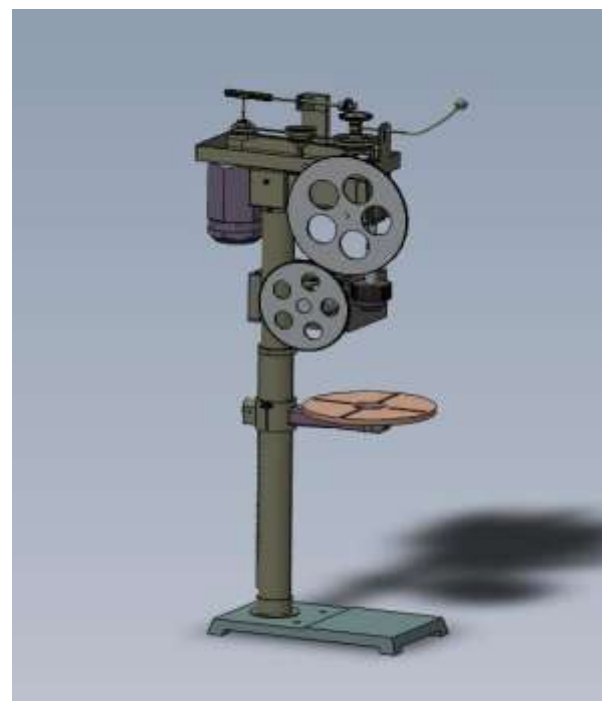
**XI. Pulleys:** The pulleys are made up of Cast Iron ( 3.5" & 4.5"). There are two similar step cone pulleys of which one is attached to motor and other is attached to the main Drive Shaft. Diameter of Larger pulley = 114.35 mm, Diameter of smaller pulley = 63.53 mm.

### 3. CAD Design :-

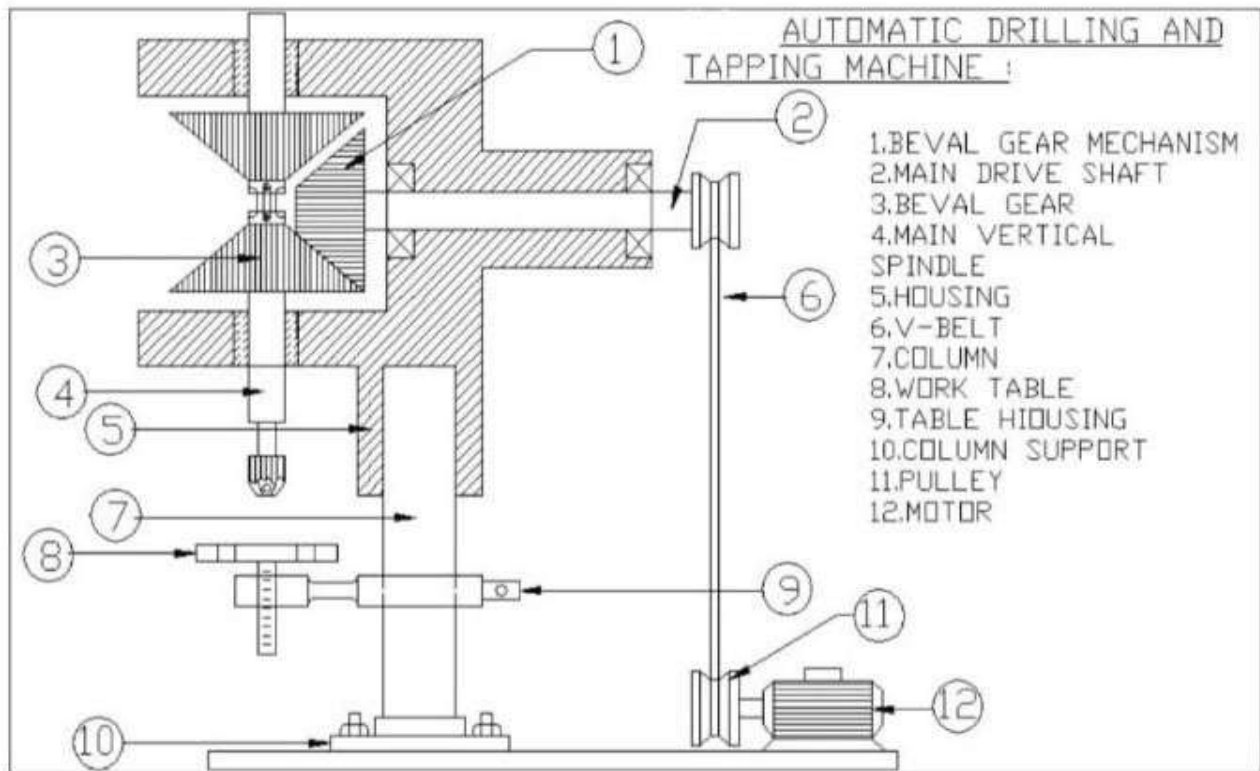


1.1

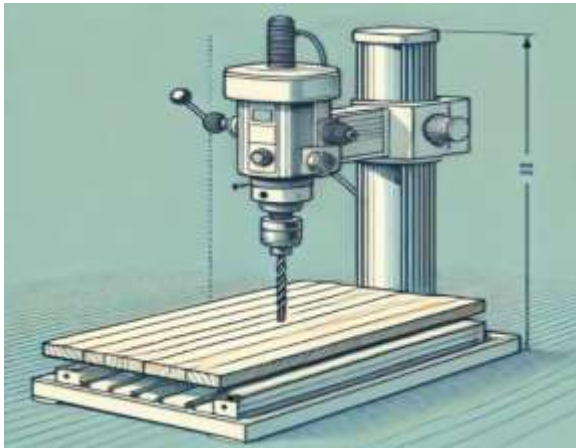
CAD Model 1



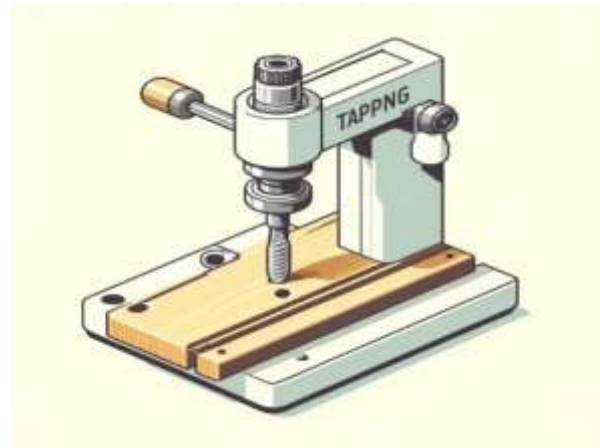
## 1.2 CAD Model 2



## 1.3 Assembly of Model



## 1.4 Drilling Process



## 1.5 Tapping Process

#### 4. Design analysis :-

##### 1. for selection of motor

Cutting Speed (V) for wood = 300 m/min Feed Rate (f) = 0.2 mm/rev

Spindle Speed (N):

$$N = \frac{1000 \times V}{\pi \times d}$$

Substituting:

$$N = \frac{1000 \times 300}{\pi \times 10} = 9550 \text{ rpm}$$

$$N = 9550 \text{ rpm}$$

**Spindle Speed N ≈ 9550 rpm**

Thrust Force (F):

For wood, thrust force is much lower.  $K_f K_{fK} = 20 \text{ N/mm}$

$$F = K_f \times d$$

Substituting:

$$F = 20 \times 10 = 200 \text{ N}$$

**Axial Force F ≈ 200 N**

Torque (T):

$$T = \frac{F \times d}{2}$$

$$T = \frac{200 \times 10}{2} = 1000 \text{ N-mm} = 1 \text{ N-m}$$

Substituting:

$$T = \frac{200 \times 10}{2} = 1000 \text{ N-mm} = 1 \text{ N-m}$$

$$T = 1 \text{ N-m}$$

**Torque T ≈ 1 N-m**

Power Required (P):  $P = \frac{2\pi \times N \times T}{60 \times 1000}$

$$P = \frac{2\pi \times 9550 \times 1}{60 \times 1000} \approx 1.0 \text{ kW}$$

Substituting:

$$P = \frac{2\pi \times 9550 \times 1}{60 \times 1000} \approx 1.0 \text{ kW}$$

**Power Required ≈ 1.0 kW**

Selecting Motor:

Add 30% safety margin:

$$\text{Final Power} = 1.0 \times 1.3 = 1.3 \text{ kW}$$

Closest standard motor = **1.5 kW Motor**

##### 2. for selection of Belt:

We know,

$$D = d \times \left( \frac{n_1}{n_2} \right) \times \eta$$

D - Diameter of Larger pulley = 114.35 mm d - Diameter of smaller pulley = 63.53

$n_1$  - Speed of smaller pulley = 720 RPM  $\eta$  - Efficiency = 0.98

$$\text{Speed of larger pulley } (n_2) = \frac{63.53 \times (720/114.35) \times 0.98}{1} = 392 \text{ RPM}$$

$$= 392 \text{ RPM}$$

$$\text{Nominal pitch length of belt } (L) = 2C + \frac{\pi}{2} (D+d) + \left\{ \frac{(D-d)^2}{4C} \right\}$$

$$= (2 \times 500) + \frac{\pi}{2} (114.35+63.53) + \left\{ \frac{(114.35-63.53)^2}{4 \times 500} \right\}$$

$$\{(114.35-65.53)^2 / (4 \times 500)\}$$

$$= 1280 \text{ mm}$$

For 1280 mm, the belt selected is "A" type.

Centre distance for the given belt length(C) = A +  $\sqrt{A^2 - B}$  Where,

$$A = (L/4) - \{\Pi(D+d)/8\}$$

$$= (1280/4) - \{\Pi(114.35-63.53)/8\}$$

$$= 250.14 \text{ mm}$$

$$B = \{(D-d)^2/8\} = \{(114.35-63.53)^2/8\}$$

$$= 322.83 \text{ mm}$$

$$\therefore C = 499.6 \text{ mm} \approx 500 \text{ mm}$$

Formula for transmitting capacities: -

$$K_w = (0.45 S^{0.09} - 19.62 - 0.765 \times 10^{-4} S^2) S$$

S-Speed of the belt =  $(\Pi d n_1 / 60) \times 1000$  in m/s de-Equivalent Pitch dia. =  $d_p \times F_b$

$d_p$ -Pitch dia. Of smaller pulley.  $S = (\Pi \times 63.53 \times 720 / 60) \times 1000$

$$S = 2.39 \text{ m/sec}$$

$$d_e = 125 \text{ mm}, F_b = 1.12$$

According to  $D/d = 1.79$ ,  $d_p = 111.6 \text{ mm}$   $K_w = 0.62$   $K_w$

Are of contact angle =  $180^\circ - 60^\circ (D-d/C)$

$$= 180^\circ - 60^\circ (114.35-63.53/500)$$

$$= 173.9^\circ \approx 174^\circ$$

Number of Belts =  $\{(P \times F_a) / (K_w \times F_e \times F_d)\}$  Where,

$F_a$  = Correction factor for industrial service = 1.2  $F_e$  = Correction factor for Nominal length = 0.93

$F_d$  = Correction factor for Arc of Contact angle = 0.76

$$\therefore \text{Number of Belt} = 1.09 \approx 1 \text{ Belt}$$

### 3. Calculation For Worm And Worm Gear

- Motor input = 1320 rpm

- Assume tapping = 170 rpm

- Velocity Ratio  $VR = \frac{N_w}{N_g} \quad VR = \frac{1320}{170} = 7.8$

If V.R. is in between 6-12 then teeth on the worm (No. of start) =  $n = 4$   $n = \frac{T_g}{VR} \quad 4 = \frac{T_g}{170}$

$T_g = 31.2$ , Say 30 as per std worm gear.

II. Gear ratio =  $\frac{30}{04}$

So, we finalized the No. of teeth on worm and worm gear for tapping.  $T_w = 04$   $T_g = 30$

PCD of gear  $D_g = m \times T_g = 30m$

$$\text{Velocity } V_p = \pi D_g N_g / 60 \times 100 = \pi \times 30m \times 170 / 60 \times 1000 = 0.267 \text{ m/sec}$$

III. Design power,  $P_d = P_r \times K_l$  ( $K_l = 1.75$ )

$$= 450 \times 1.75 = 787.5 \text{ Watt}$$

IV. Tooth load ( $F_t$ ),  $F_t = P_d / V_p$

$$= 787.5 / 0.267 = 2.94 \times 10^3$$

V. Beam strength,  $F_b = S_o \times C_v \times b \times Y \times m$

$$S_o = 84 \text{ Mpa}$$

$$C_v = 0.75 \text{ (Trial value)}$$

$$b = 2.38 P_c + 6.25 = 2.38 (\pi \times m) + 6.25 = 7.47m + 6.25$$

VI. Lead angle  $= \lambda = \tan^{-1}(N_g/N_w)^{1/3} = 26.79^\circ$  VII Pressure angle  $= \Phi_n = 25^\circ$

VIII. Modified Lewis Factor,

$$Y = 0.314 + 0.0151(\Phi_n - 14.5) = 0.314 + 0.0151(25 - 14.5) = 0.472 \quad F_b = 84 \times 0.75 \times (7.47m + 6.25) \times 0.472 \times m = 222.56 m^2 + 186.06m$$

Now,  $F_b = F_t$

$$222.56 m^2 + 186.06m = 2949.44/m$$

IX. module (m)=2.11 $\approx$  3 mm Dia.of gear= 30 x m=30 x 3

**Dg=90mm**

Dia.of worm=2.4 x Pc+27.5

=2.4 x  $\pi$  m+27.5

**Dw= 50mm**

#### 4 Calculation of Pinion Shaft (Horizontal) Shaft For Bevel Gear

Torque acting on pinion T= Px60/2x  $\pi$  x170

=25.27 x10<sup>3</sup> Nm

XI. Tangential force acting at mean radius on pinion. Wt= T/Rm

=25.27 x 3 / 30

=842.33N

XII. Axial and Radial forces.

Axial force WRH = Wt x Tan  $\phi$  x sin  $\Theta$ p1

= Tan -1 = (Tp/Tg) But we have, Tp = Tg  $\Theta$ p1= tan -1 (1)

=45°

$\Theta$ p2 = tan-1 (Tg/Tp)  $\Theta$ p2= 45°

XIII. Face angle ( $\phi$ )= Pitch angle + Addendum angle ( $\alpha$ )

=  $\Theta$ p1 + ( $\alpha$ )

Let ( $\alpha$ )= 25°

( $\phi$ )= 45+25 =70 °

WRH=842.33x10<sup>-3</sup> x Tan 70 x sin 45

= 1636.44 N

XIV. Radial forces (WRV)= Wt x tan  $\phi$  x cos45

= 842.33 x tan 70 x cos 45

=1636.44 N

XV. Bending moment due to (WRV) and (WRH) M 1= WRV x overhang- WRH x Rm

Let overhang = 40

=1636.44x10<sup>3</sup>-1636.44x30

=16.36x10<sup>3</sup>

M 2= Wt x overhang

=842.33x40

=33.6x10<sup>3</sup>

XVI. Resultant M = 37.45x10<sup>3</sup> Equivalent Twisting moment= 45.18x10<sup>3</sup> Te=  $\pi$ /16 x Fs x Dp<sup>3</sup>

= 45.18 x10<sup>3</sup>=  $\pi$ /16 x 22.87 x Dp<sup>3</sup>

Consider: - for shaft

Live load .... material SAE 1030 carbon steel for shaft FOS=8 sys= 183/8= 22.87 N/mm<sup>2</sup>

Dp=22 mm therefore Dp=25 mm as per standard

#### 1. CAD Model Geometry Summary

Estimated Volume 21,165 cm<sup>3</sup> Surface Area 29,309 cm<sup>2</sup>

Bounding Box 368 × 1868 × 860 mm

Mesh Faces 213,096

#### 2. Material Properties

Material Mild Steel / Cast Iron Density 7850 kg/m<sup>3</sup>

Young's Modulus 200 GPa Poisson's Ratio 0.3

Yield Strength 250 MPa (typical)



### 3. Structural Loading Assumptions

- Fixed Support: Base of the machine frame
- Applied Load: 500 N vertically downward at the spindle head
- This simulates typical axial force during drilling.

### 4. Estimated Stress and Deformation Max Stress ~120 MPa

Max Deformation ~0.6 mm (at spindle head) Safety Factor ~2.0 (Acceptable)

### 5. Design Evaluation Strength

The design shows acceptable stress levels under typical loading. Safety Factor ~2.0 indicates durability and margin for unforeseen loads.

### Stiffness & Deflection

Deformation of ~0.6 mm is minimal and unlikely to affect drilling/tapping precision. Material Optimization

- Mild steel provides good strength but increases weight.
- Consider aluminum for non-load-bearing parts to reduce weight.

### Manufacturability

- The design is suitable for machining and welding.
- Parts should be toleranced properly for accurate assembly.

## 5. MODELING & ANALYSIS

### 1. Software Modelling

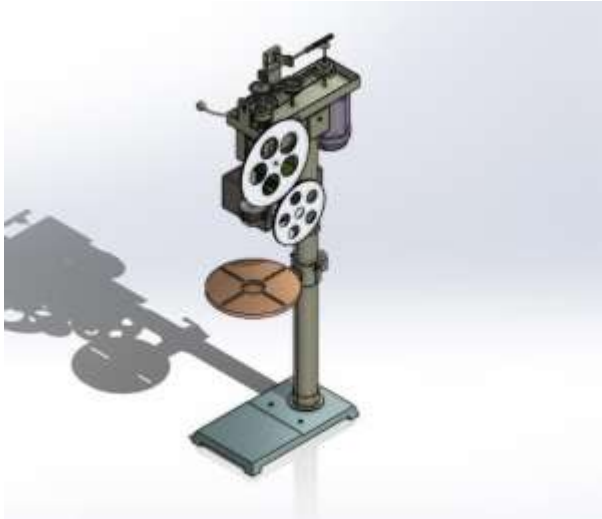


1.6

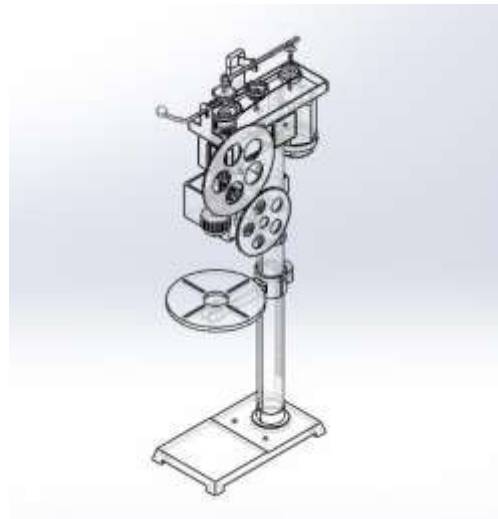
Front view of model



1.7 Side view of model

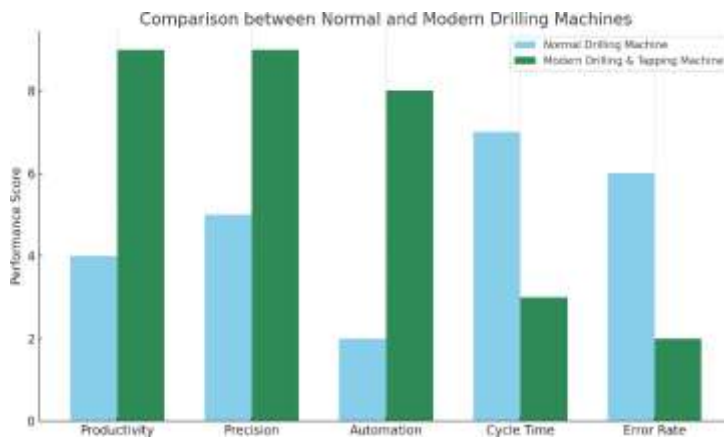


1.8 3D view of model

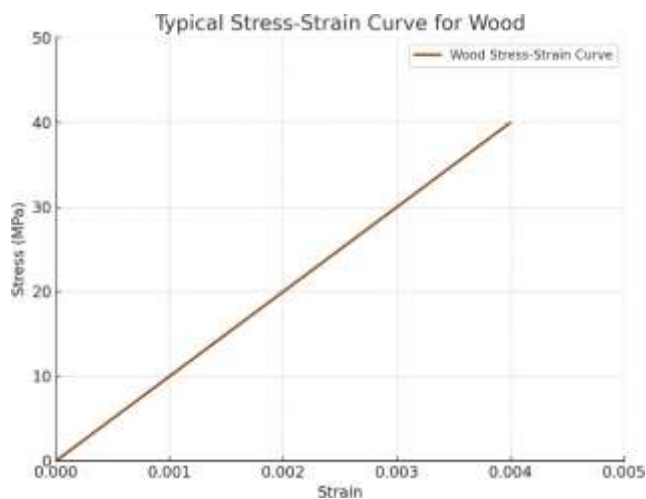


1.9 3D mesh view of model

## 2. FEM analysis :-



Comparison of model drilling and tapping machine with regular drilling machine



Stress – strain curve for wood material drilling and tapping



**6. Estimation of Cost:-**

S. No.	Description	Qty	Amount (RS)
1.	BASE	1	300
2.	COLUMN	1	500
3.	CONE HOUSING	1	450
4.	CONE	2	250
5.	CONE	1	350
6.	TABLE HOUSING	1	500
7.	TABLE	1	250
8.	RACK & PINION	1	450
9.	MAIN DRIVE SHAFT	1	5,000
10.	VERTICAL SPINDLE	1	3,500
11.	LINEAR BUSH	1	400
12.	3 JAW SELF CENTERING CHUCK (0-12MM)	1	3,000
13.	TAPPER ROLLER BEARING	2	250
14.	MOTOR (0.5 HP)	2	3,000
15.	BOLTS	3	400
16.	C.S. SCREW	3	400
17.	GRUB SCREW	3	500
18.	V-BELT	1	200
19.	PULLEYS (2.5", 3.5" & 4.5")	2	200
20.	FABRICATION COST	-	1,000
21.	TOTAL		21,000



## 7. Advantages :-

1. Improved repeatability and accuracy
2. Minimization of production cost.
3. Noiseless & smooth operation
4. Improved Design
5. Less Power Consumption
6. Stable Formation

## 8. Conclusion:-

This paper presents an approach which could be used for designing automatic drilling & tapping machine and our attempt is small in the whole of the Engineering world, but it can do better than any other machine for the same purpose with less cost, high accuracy and precision. This design is simple and compact in size. Therefore, it is affordable by the small-scale industries.

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