

Design & Analysis of Non-Linear Property of Material for Semi-Rigid, Fixed & Flexible Structural Frames

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Abstract -During an earthquake, failure of structure starts off-evolved at factors of weak spot. This weak point arises due to discontinuity in mass, stiffness and geometry of structure. The systems having this discontinuity are termed as irregular systems. Irregular structures contribute a massive portion of city infrastructure. The effect of vertically irregularities within the seismic overall performance of systems will become definitely vital. The main objective of the analysis is to study the behavior of flat slab system in vertical irregular multi-storied building against different forces acting on it during earthquake. Also, the objective of analysis is to study the structural behavior of shear wall – flat slab interaction with opening. The analysis is made between in the three types of G+9 storey building with 0 % vertical irregularity, 200 % vertical irregularity and 300% vertical irregularity. In all these building's shear wall is provided with & without 20% opening. Total 15 modeled are studied and their results were compared.

Key Words: Flat slab, Vertical Geometric Irregularity, Shear wall with opening, Response Spectrum analysis, STAAD Pro2007

1. INTRODUCTION

It is assuming that the analysis of steel portal frames that beam-to-column connections are rigid and for trusses joints are pinned. Rigid connections, where no relative rotations occur between the connected members, transfer not only a significant amount of bending moments, but also shear and axial forces. Despite these facts, it is largely recognized that the great majority of joints does not exhibit such idealized behavior. These connections are called semi-rigid, and their design should be performed according to their actual structural behavior.

This thesis presents a semi-rigid low-rise portal frame nonlinear dynamic analysis. The main objective of this study is to propose a modelling strategy to represent the dynamical behaviour of semi-rigid joints under dynamic actions implemented on the SAP 2000 software.

The developed model included the material non-linearity and considered the influence of non-linear connection stiffness.

Types of Semi-Rigid Connections

- i) Single web-angle and single plate connections
- ii) Double web-angle connections
- iii) Header plate connection
- iv) Top and seat-angle connection
- v) Extended/Flush end plate connections
- vi) T-stub connections

2. ANALYSIS OF SEMI RIGID CONNECTION

A steel beam ISMB300 having length 6 m is used uniformly distributed load is 10 kN over total span. Analysis done with the help of SAP2000 as flexible, semi-rigid and rigid. First analysis done on simple beam (Figure 1) without semi-rigid connection to compare the results. We know that properties of semi-rigid connections are in between the flexible and rigid connections. To find the stiffness of semi-rigid connection the concept of End fixity factor was used. We know that the end fixity factor, r is 0 for flexible connection and 1 for rigid connection. For semi-rigid connections the end fixity factor lies somewhere 0 to 1. By using relation between stiffness and end fixity factor the stiffness's for end fixity factor 0.1, 0.2, 0.3,0.9 are find out and analysis are done for these stiffness's. Stiffness assign to the link is 8604 kN/rad.

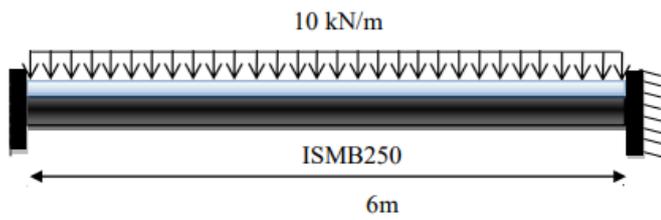


Figure 1 Fixed beams with UDL Stiffness

Following table gives the comparison between the structure with and without semi-rigid connection in beam.

Table 1 Results obtained for beam with UDL

| Results for | Flexible connection | Rigid connection | Semi-rigid connection |
|-----------------------|---------------------|------------------|-----------------------|
| Maximum +ve BM, (kNm) | 46.95 | 15.65 | 28.17 |
| Maximum -ve BM, (kNm) | - | 31.30 | 18.28 |
| Shear force, (kN) | 31.3 | 31.3 | 31.3 |
| Frequency, (rad) | 26.59 | 50.8 | 35.41 |

Following are the moment v/s End fixity factor and frequency v/s End fixity factor curves of semi-rigid beam

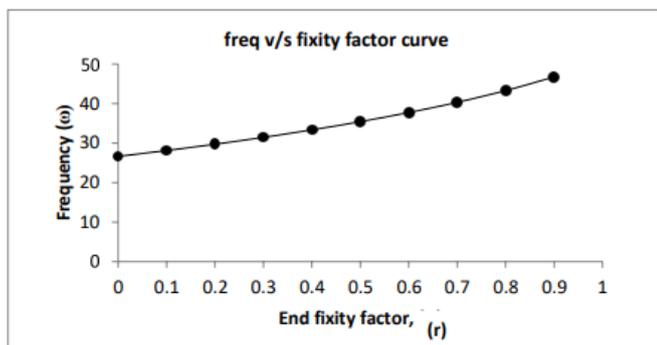


Figure 2 Natural frequency vs end fixity factor

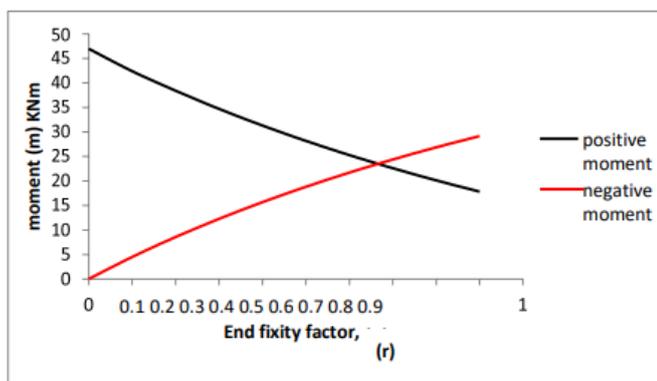


Figure 3 Moment vs end fixity factor

3. CALCULATION OF STIFFNESS

Stiffness is calculated by using following relations. As per IS 800: 2007

Table 2 Connection Classification Limits

| Nature of the connection | In terms of strength | In terms of stiffness | K |
|--------------------------|----------------------|-------------------------------------|-----------------|
| Rigid connection | $m^1 \geq 0.7$ | $m^1 \geq 2.5 \theta^1$ | $K \geq 2.5$ |
| Semi-Rigid connection | $0.7 > m^1 > 0.2$ | $2.5 \theta^1 > m^1 > 0.5 \theta^1$ | $2.5 > K > 0.5$ |
| Flexible connection | $m^1 \leq 0.2$ | $m^1 \leq 0.5 \theta^1$ | $K \leq 0.5$ |

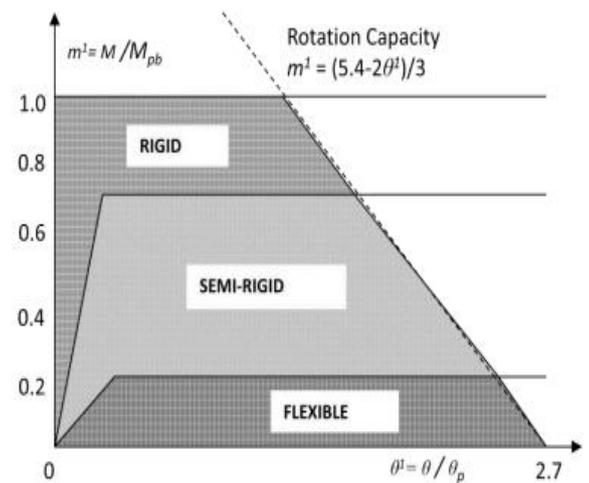


Figure 4 Classification of connection according to Bjorhovde (IS800, 2007)

4. PROBLEMS ANALYSIS

- (i) **Problem description:** Bay width = 6m Storey height = 4m
 Dead load = 10.23 KN/m
 Live load = 6 KN/m
 Beam section = ISMB200
 Column section = ISBM 600
 Plastic moment of beam, $M_p = 116.43$ KNm
 Line mass - 1.345 kg/m
 Assuming 150 mm thickness of concrete slab.
- (ii) Nonlinear analysis data: NL Link type - Plastic (Wen) Property name - Lin1
 Effective stiffness - K Effective damping - 0.02 Stiffness - K
 Yield strength - Y Post

yield stiffness ratio – 0.2, 0.5, and 0.8
Yielding exponent – 5

- (iii) **Time History Data:** The time history of Kobe earthquake considered. Time interval (DT) = 0.01 Header line to skip = 4 Prefix character per line to skip = 2 Number of points per line = 5 Number of output time step = 4096 Output time step size = 0.01

Case I & Case II Problems
Case I – Two Bay Three Storeys

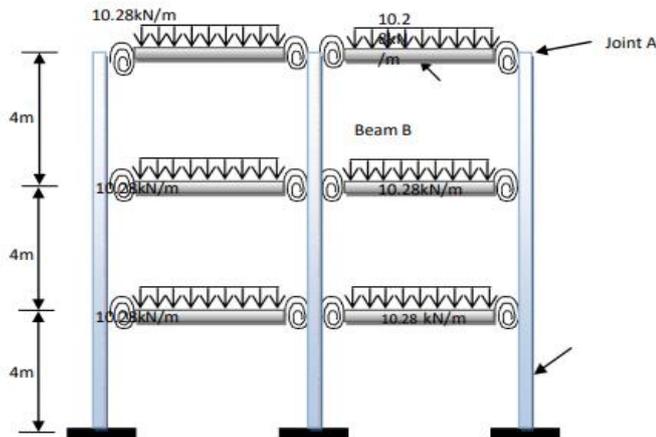


Figure 4 Two Bay Three Storey Frame

Following graphs shows frequency of building at each mode for different stiffness.

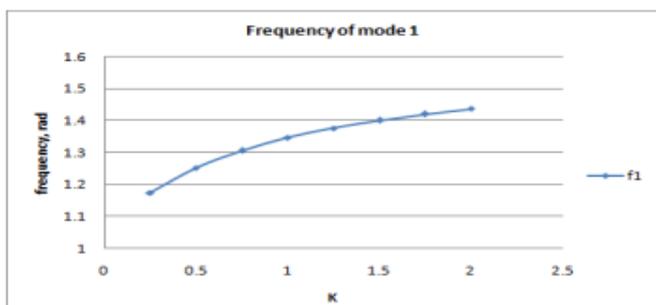


Figure 5 Variation of natural frequency of mode 1 with different stiffness

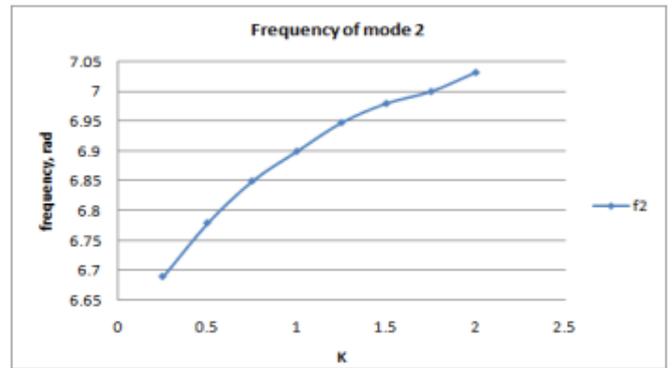


Figure 6 Variation of natural frequency of mode 2 with different stiffness

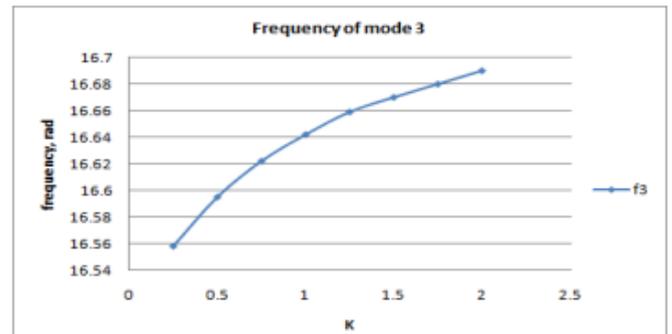


Figure 7 Variation of natural frequency of mode 3 with different stiffness

Observation:

- Frequency depends upon the Stiffness. It decreases with decrease in the value of Stiffness.
- Frequency does not depend upon the Yield strength.
- Frequency does not depend upon the Post yield stiffness ratio.

5. MODELLING CONCLUSIONS

- While modelling of semi-rigid connections in SAP2000 software the most important step is to assign the constraints to the joint because if the constraints not assigned then all the components like connections, beam and column behave independently.
- Constraints may be different for a different case like in nonlinear analysis case its assign as Translation is constrained in Y direction and free to translate and rotate in other direction. But the case may different in case of linear analysis. Hence, it is better to go for trial and error.

- For Nonlinear analysis use of plastic (Wen) link is relevant it gives good results.

ANALYSIS CONCLUSIONS

- Frequency depends upon the Stiffness. It decreases with decrease in the value of Stiffness.
- Frequency does not depend upon the Yield strength.
- Frequency does not depend upon the Post yield stiffness ratio.
- Axial force in column is largely depends upon the Stiffness as it shows large deference in the results for different value of Stiffness.
- Axial force in column is decreases with decrease in the value of stiffness.
- Axial force in column is also depends upon Yield strength of beam. It decreases with decrease in value Yield strength.
- Axial force in column is also depends upon the Post yield stiffness ratio. It decreases with decrease in value of Post yield stiffness ratio.
- In rigid case which is for 0.8 Mp & 0.7 Mp. Axial force in column shows very less increase in value with increase in Post yield stiffness ratio and hence there is not much deference show in the plotted curves refer figure 4.8.

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