

PERFORMANCE ANALYSIS OF THERMOACOUSTIC REFRIGERATION FOR AUTOMOBILE

¹Sajid Siddique, ²Huzaifa A. Fidvi, ³Aniket Wasnik, ⁴Akshay Narnawre,
⁵Prince Hirekhan, ⁶Abhay Chavan.

^{1,2}Department of Mechanical Engineering, Anjuman College of Engineering and Technology, Nagpur, India.

^{3,4,5}Student of mechanical Engineering, Anjuman College of Engineering And Technology, Nagpur, India.

Keyword :-

Refrigeration effect
Sound Waves
Vehicle air conditioning
Refrigerant or Inert gases

ABSTRACT

Concerns in regards to the natural effect related with the utilization of current fume pressure refrigeration frameworks in autos have prompted the examination of option 'green' advances. Thermoacoustic refrigeration, an arising 'green' innovation in light of the deliberate utilization of high-pressure sound waves to give cooling, is the most encouraging substitution researched up until this point. Thermoacoustic fridges utilize naturally harmless gases, are moderately basic and cheap to produce and can work utilizing an intensity source, which prompts their allure as an economical waste intensity recuperation gadget. In this paper, the plausibility of a thermoacoustic fridge driven by recuperated heat from the waste fumes gases of a car is examined. Viable contemplations and estimations integrating common execution qualities demonstrate that a car squander heat driven thermoacoustic forced air system is possibly doable and warrants further examination.

GLOSSARY OF TERMS

AHX	ambient heat exchanger
AMR	active magnetic regenerator
ATAR	automotive thermoacoustic refrigerator
CFC	chlorofluorocarbon
CHX	cold heat exchanger
COP	coefficient of performance
COP _r	Carnot relative coefficient of performance
GWP	global warming potential
HDTAR	heat driven thermoacoustic refrigerator
HHX	hot heat exchanger
TAR	thermoacoustic refrigerator
TE	thermoelectric
TEWI	total equivalent warming potential
VAR	vapour absorption refrigeration
VC	vapour compression
VMAC	vehicle magnetic air conditioner

INTRODUCTION

Thermoacoustic' refrigeration is an arising innovation 'in light of the deliberate utilization of extreme acoustic waves to siphon nuclear power into or out of a volume of liquid. This innovation offers equivalent productivity to regular frameworks, without ecologically destructive working liquids, huge support prerequisites or high development costs. Thermoacoustic refrigeration can be driven involving heat as an immediate information energy source, and as such is engaging for squander energy recuperation from heat sources, for example, hot fumes gas streams from existing thermodynamic cycles.

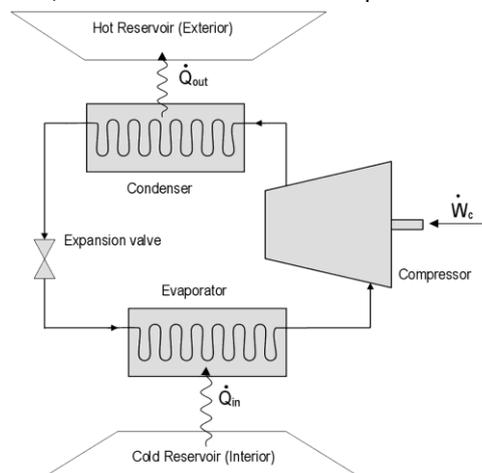
Current refrigeration and cooling frameworks for autos are fume pressure frameworks, which have been ceaselessly evolved and refined since their origin during the 1930s. They work by an intensity move process that happens while a functioning liquid is compacted and extended. Fume pressure frameworks are surely known, dependable, and minimized. Despite the fact that fume pressure frameworks are generally utilized in the car business, the blower draws critical power from the motor, which diminishes the generally productivity of the vehicle. The refrigerant frequently spills from the climate control system into the environment, and is a supporter of an Earth-wide temperature boost.

Propels in the improvement of thermoacoustic refrigeration could give an elective answer for cooling vehicles which could utilize hot exhaust gases as an energy source. A thermoacoustic fridge needn't bother with a blower, and consequently brings down fuel utilization, expands the accessible motor power and in general framework effectiveness. Thermoacoustic fridges can utilize effectively possible honorable (dormant) gases as a functioning liquid, which represent an essentially decreased natural effect contrasted with R-134a and R-22 refrigerants utilized in present day fume pressure frameworks. Furthermore, the development of thermoacoustic coolers is somewhat basic, possibly bringing about a lower evaluated framework contrasted with a fume pressure framework, and essentially disposing of continuous upkeep costs.

This paper contains a conversation of the plausibility of a thermoacoustic refrigeration framework in a car application fueled by the waste intensity present in a vehicle's fumes. Initial, a correlation will be made between fume pressure frameworks and different frameworks viewed as option car refrigeration frameworks with less ecological effect. Following this, the essential activity of a thermoacoustic framework is explored. A few key contemplations with respect to the waste intensity accessible from vehicle depletes and in the plan of a car thermoacoustic fridge is then examined.

Fume Pressure Refrigeration Frameworks

Current auto cooling and refrigeration frameworks depend on the fume pressure (VC) refrigeration cycle as displayed in Figure 1, which is a non-ideal type of the Carnot refrigeration cycle. Auto cooling frameworks in light of the VC cycle have been being developed since the 1930s (Bhatti 1999b). In a car VC cooling framework, a refrigerant is extended to such an extent that it eliminates heat from an intensity exchanger in the return air pipe to the vehicle inside, and compacted in a rotational blower to convey intensity to an intensity exchanger outside the vehicle inside. Pressure is regularly accomplished by drawing power from the motor driving rod. Development of the refrigerant is given by the utilization of a basic one-way choking valve. Heat exchangers are probably going to be finned-tube radiators, with current models developed from aluminum.



Source: adjusted from Moran and Shapiro (2000:517)

Figure 1. Fundamental parts of a fume pressure cycle.

Refrigerants

For north of fifty years until the mid 1990s, the most well-known refrigerant in VC cycles was the chlorofluorocarbon (CFC) Refrigerant 12, named 'R-12' (Moran 2000). The presence of chlorine in R-12 (and furthermore in the generally utilized Refrigerant 22) was viewed as a significant supporter of consumption of the ozone layer in the world's air when delivered. Refrigerant 22, another normal refrigerant named 'R-22', is broadly utilized in VC frameworks and offers diminished natural effect by supplanting a portion of the chlorine particles with hydrocarbons (Moran 2000). In an ever-evolving create some distance from refrigerants with a high potential for ozone layer consumption, Refrigerant 134a (R-134a) was acknowledged as a trade for R-12 in the mid 1990's (Brown 2002).

There are a different scope of elective cooling refrigerants viable for use in VC frameworks. Alkali, propane and methane are being scrutinized as substitutions; but the poisonousness of smelling salts and the combustibility of propane and methane request cautious thought in plan.

Brown et al. (2002) remark serious areas of strength for on endeavors into CO₂ in the last part of the 1990's. The utilization of CO₂ as a refrigerant was normal in the nineteenth 100 years, and it is presently a possible swap for R-134a. CO₂ has an unnatural weather change potential multiple times not as much as R-134a and multiple times not as much as R-12 (Bhatti 1999a), and in 1998, Gentner (1998) showed that in contrast with R-134a frameworks, CO₂ frameworks in traveler vehicles had satisfactory proficiency and cooling power limits. Nonetheless, Bhatti (1999a) contended that despite the fact that CO₂ (as a delivered gas) has a diminished an unnatural weather change potential than R-134a, the expansion in fuel consumed to make up for the diminished effectiveness and expanded load of an identical CO₂ framework would really prompt more prominent an Earth-wide temperature boost influence. Comparable contentions have been made for VC frameworks involving air as the refrigerant.

Other Drawbacks

Significantly, the unfavorable impacts and contamination created by petroleum and diesel motors are intensified by the extra burden forced by the blower, since the blower draws valuable mechanical power from the result of the vehicle motor. Fume pressure refrigeration frameworks are perplexing and furthermore require many parts disseminated all through the vehicle, associated with one another by means of a compressed refrigerant circuit. Notwithstanding the four primary parts as displayed in Figure 1, current auto frameworks likewise use what is alluded to as an 'aggregator' between the evaporator and blower. The collector is utilized to contain the blended fluid/gas periods of the refrigerant with the end goal that the blower draws just the fume stage. Blowers are cumbersome, require the utilization of greases and seals, and a defective strain sensor or spillage in the collector or any part of the framework can prompt quick wear and disappointment of the blower.

ALTERNATIVE AUTOMOTIVEREFRIGERATION SYSTEMS

Endeavors to address disadvantages in the utilization of fume pressure refrigeration frameworks incorporate the advancement of elective refrigeration frameworks other than thermoacoustics. A few of the most encouraging elective advancements to fume pressure and thermoacoustic refrigeration frameworks are fume retention, strong adsorption, dynamic attractive regenerator, and thermoelectric refrigeration frameworks and they are examined in the accompanying segments.

Fume Retention Refrigeration Frameworks

Figure 2 shows a Fume Retention Refrigeration (VAR) framework. This framework contrasts from fume pressure refrigeration frameworks in that heat itself is utilized to pack the functioning liquid, rather than pressure by mechanical work. Energy conveyed to the generator is utilized to warm the functioning liquid to a fume and 'siphon' it at high-strain and temperature to the condenser, where it rejects intensity to its cooler environmental elements. Fluid refrigerant leaving the condenser is choked to a low tension and at its coldest state in the cycle, acknowledges heat from the vehicle inside by means of the evaporator. The fluid refrigerant is then gotten back to the safeguard (and to the generator by means of the little mechanical siphon) to go full circle.

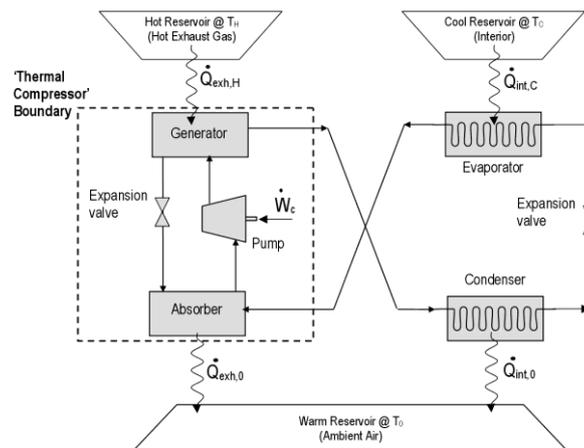


Figure 2. Diagram of a single-stage vapour-absorption refrigeration (VAR) cycle using an exhaust gas stream as an energy source.

Minimal mechanical work is expected to work the VAR cycle. The functioning liquid is generally a smelling salts water or lithium-bromide arrangement in water, which as a fluid is coursed with more prominent tantamount proficiency than compacted gas. Smelling salts water frameworks were first evolved around the beginning of the twentieth hundred years with the lithium-bromide frameworks

around since the 1950's (Johnson 2002), which proposes there is as of now some assembling reason for improvement of a car application.

In any case, VAR frameworks are bulkier, more costly, heavier and less productive than VC frameworks (Steward 2001). There is greater gear in a VAR framework contrasted with a fume pressure framework, a greater expense that is monetarily supported just when a reasonable measure of in any case squandered heat is accessible (Johnson 2002). Moreover, the more prominent load of the VAR framework requires extra power from the motor to move the vehicle. The utilization of smelling salts and destructive lithium bromide require extra plan contemplations: smelling salts is harmful and represents a gamble to somewhere safe whenever spilled; lithium bromide is destructive and makes hydrogen gas when it contacts ferrous regulation frameworks (Johnson 2002) which influences the framework effectiveness.

Strong Adsorption Cooling Frameworks

Two kinds of strong adsorption cooling cycles, Metal Hydride and Zeolite, have both been effectively determined by hot fumes gas streams (Johnson 2002).

Metal Hydride frameworks work utilizing two beds or stack of two distinct metal hydrides, and three intensity exchangers, at hot, cold and encompassing temperatures. Metal hydrides are metallic mixtures which delivery heat after retaining hydrogen, and consume heat after delivering hydrogen. Since the exhibitions of metal hydrides are temperature-dependant, run of the mill metal hydride frameworks utilize a high temperature (for example $ZrCrFe_{1.1}$, $LaNi_{4.75}Al_{0.25}$) and a low temperature hydride (for example $LaNi_5$, $MmNi_{4.15}Fe_{0.85}$) (Johnson 2002) coordinated.

Utilizing two beds of such metallic mixtures, with one at a higher temperature than the other, heat is consumed from the hot intensity exchanger (fumes gas stream) into the high-temperature hydride, which after getting heat, discharges hydrogen into the low-temperature hydride, which thus delivers intensity to the surrounding heat exchanger. The cushions are then moved, to such an extent that the high-temperature cushion is at the surrounding heat exchanger and the low-temperature cushion is at the virus heat exchanger. This plan permits intensity to enter the low-temperature hydride, which returns the hydrogen to the high-temperature hydride, which after getting the hydrogen discharges intensity to the encompassing intensity exchanger. The interaction is then rehashed; but a couple of cushions could be utilized to draw heat from both the hot and cold intensity exchangers ceaselessly.

Zeolite frameworks have higher efficiencies than metal-hydride frameworks, and zeolite materials are economical to get: the expense of sufficient metal hydride for a 2-cushion refrigeration unit going from US\$74 to US\$360 (Johnson 2002). Zeolite frameworks are

likewise non-harmful, non-combustible and irrelevantly destructive, but trouble exists in their plan because of the unfortunate warm conductivity of zeolite materials themselves (Lang 1999). The mass of zeolite frameworks appear to be like fume pressure frameworks with explicit cooling power densities around 0.1-0.3kW/kg (Wang 2002).

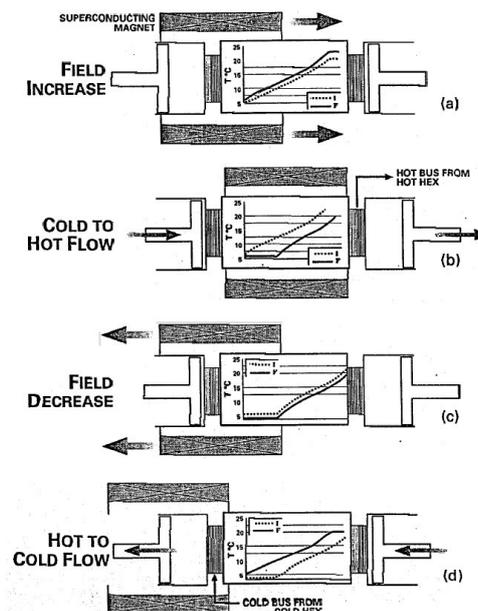
Dynamic Attractive Regenerator Frameworks

Dynamic Attractive Regenerator (AMR) frameworks work on a basic level as displayed in Figure 3 by utilizing an attractive component to charge and demagnetize an attractive 'refrigerant,' and a permeable bed through which an intensity move liquid streams. The framework utilizes a magneto-caloric impact in the strong refrigerant, by which the expansion and expulsion of the attractive field increments and diminishes the temperature of the refrigerant separately. Charge is accomplished by moving the superconducting attractive sleeve over the strong refrigerant. A fluid coolant, for example, water is siphoned into the permeable refrigerant with reasonable timing with the attractive sleeve to such an extent that fluid streams from cold to hot while the refrigerant is polarized as well as the other way around. Utilizing this standard, the strong refrigerant serves as a regenerator with high surface contact regions. Gschneidner et al. (2002) portray an auto utilization of the innovation alluded to as the Vehicle Attractive Climate control system (VMAC).

The significant advantages of AMR innovation is that as with thermoacoustic frameworks, there are no earth destructive refrigerants and efficiencies are higher than tantamount VC refrigeration frameworks (Head servant 2001). The permeable attractive bed is a strong which can only with significant effort get away from the framework, and the intensity move medium is a fluid, which can be siphoned with more noteworthy productivity than gases. Gschneidner et al. (2002) contend that the cycle could bring about Carnot efficiencies drawing nearer 100 percent. Practically speaking the proficiency is under 100 percent and the fundamental plan of Gschneidner et al. was supposed to create 1kW of cooling power at 30% Carnot proficiency.

The two most restricting issues with AMR innovation are mass and cost. The 2002 concentrate by Gschneidner et al. observed that their VMAC was 2 to multiple times heavier than identical limit VC refrigeration frameworks. Besides, Head servant (2001) states that while dynamic attractive refrigeration is more effective than VC frameworks, the innovation is as yet cost-restrictive for building applications, where in contrast with car applications, the heaviness of the framework is evidently immaterial.

Figure 3. Sketch of the active magnetic regenerator systemcycle



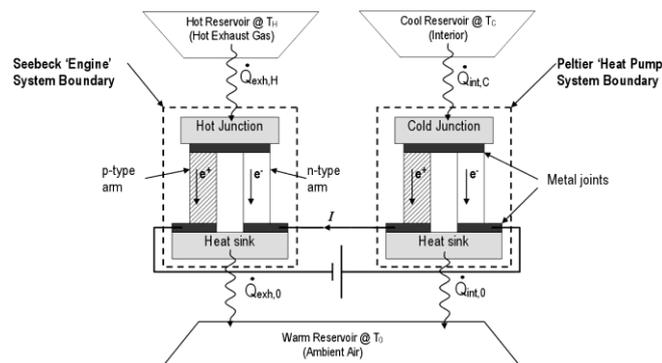
Thermoelectric Gadgets

Thermoelectric (TE) gadget improvement ostensibly started in the mid nineteenth hundred years, when Seebeck (1822) showed changes in the electrical possible across an intersection of two divergent metals when a warm slope was applied to the intersection. Presently named the Seebeck Impact, this peculiarity is utilized overall as a precise type of temperature estimation, where such tests today are by and large named 'thermocouples'.

Peltier (1834) tracked down signs that the opposite was valid; use of an electric likely across an intersection of two different metals brought about a temperature contrast across the intersection not in concurrence with Joule warming. Lenz (Ioffe 1957) showed the consequences of Peltier's analyses were to be sure because of the converse of the Seebeck impact, and this type of TE cooling has since been alluded to as the Peltier Impact.

Figure 4. Sketch of Peltier cooler powered by a Seebeck generator

Figure 4 shows a reasonable joined Seebeck ('Motor') and Peltier ('Intensity Siphon') framework, where electrical power extricated



from the hot fumes gas by the Seebeck gadget is utilized to drive a Peltier thermoelectric climate control system. The 'motor' and 'intensity siphon' demonstrated in Figure 4 are demonstrated to be indistinguishable in development yet inverse in use.

Peltier-Seebeck thermoelectric gadgets have exceptionally beneficial characteristics for car refrigeration in their versatility, flexibility, unwavering quality and absence of refrigerants.

The best deficiency with the utilization of Peltier thermoelectric gadgets is their unfortunate warm effectiveness, which for the best TE material blends (working at room temperature) is under 10% Carnot proficiency (DiSalvo 1999). Enhancements in the productivity of TE gadgets has been as a matter of fact delayed since the 1950's, in generally part because of limits in the thermoelectric properties of accessible materials.

An intriguing similar concentrate between fume pressure, fume ingestion and thermoelectric fridges by Bansal and Martin (2000) featured the shortcoming of thermoelectric frameworks at a business item level. The refrigeration frameworks tried were all industrially accessible little lodging coolers of comparative limit, worked to keep an ice chest inside temperature of 5°C. The deliberate in general coefficient of execution of the TE cooler was 0.66, a COP very nearly multiple times not exactly the fume pressure framework (2.59), but still an outcome better than that of the fume retention framework (0.47).

Relative Outline of Elective Refrigeration Frameworks

Table 1 gives a straightforward correlation of the advantages presented by every elective refrigeration framework to fume pressure (VC) refrigeration frameworks, as far as relative expense to fabricate, all out identical warming effect (TEWI) (Bhatti 1999a) relative coefficient of execution (COP_r), unit weight, and power thickness.

Table 1. Comparison of Refrigeration Systems.

System	Cost	TEWI	COP _r	Weight	Power Dens
VC	OK	Poor	Good	Good	V. Good
VAR	Poor	Good	Poor	Poor	OK
Metal Hyd.	V. Poor	Good	Poor	OK	Poor
Zeolite	OK	Good	OK	OK	OK
AMR	Poor	Good	V. Good	Poor	OK
TE	Good	V. Good	V. Poor	OK	Poor
TA	V. Good	V. Good	Poor	Good	OK

THERMOACOUSTIC REFRIGERATION

The term 'thermoacoustic' is much of the time utilized regarding the perception that such frameworks convert heat power into acoustic power as well as the other way around. Nonetheless, thermoacoustic frameworks so far developed to date are likewise a mind boggling utilization of both thermodynamic and acoustic hypothesis.

Thermoacoustic frameworks can be isolated into two distinct classes - 'heat motors' (otherwise called 'central players') and 'intensity siphons'. On a fundamental level, heat motors take heat energy from a hot repository, convert a portion of the intensity energy into acoustic energy and dump the unused intensity to a cool supply. Heat siphons utilize acoustic energy to siphon heat starting with one temperature repository then onto the next, bringing about a temperature inclination between the two supplies.

Thermoacoustic fridges are commonly determined either by a gas relocation framework (like an amplifier) or a thermoacoustic heat motor that creates high plentifulness sound. Amplifiers or electrodynamic shakers convert electrical power into acoustic power, are moderately simple to execute and can be reasonable. In examination, thermoacoustic heat motors have regularly higher acoustic efficiencies. These gadgets likewise don't have moving parts, which proposes a long help existence with no support. Trial heat motors usually utilize resistive warming components to change over electrical power into nuclear energy, which the intensity motor proselytes into acoustic power.

Figure 5 shows a framework graph for a car thermoacoustic cooler (ATAR), in which the waste intensity $Q_{exh,H}$ is utilized by an intensity motor to create acoustic power W_{acous} , which is then conveyed to an intensity siphon to separate intensity $Q_{int,C}$ from the vehicle inside. As displayed in Figure 5, the significant wellsprings of intensity entering the vehicle inside are the convective and brilliant intensity loads from the outside climate, and the intensity delivered by the vehicle tenants.

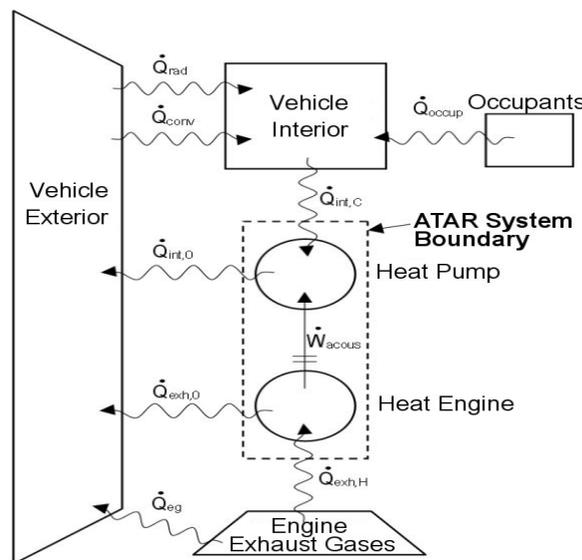
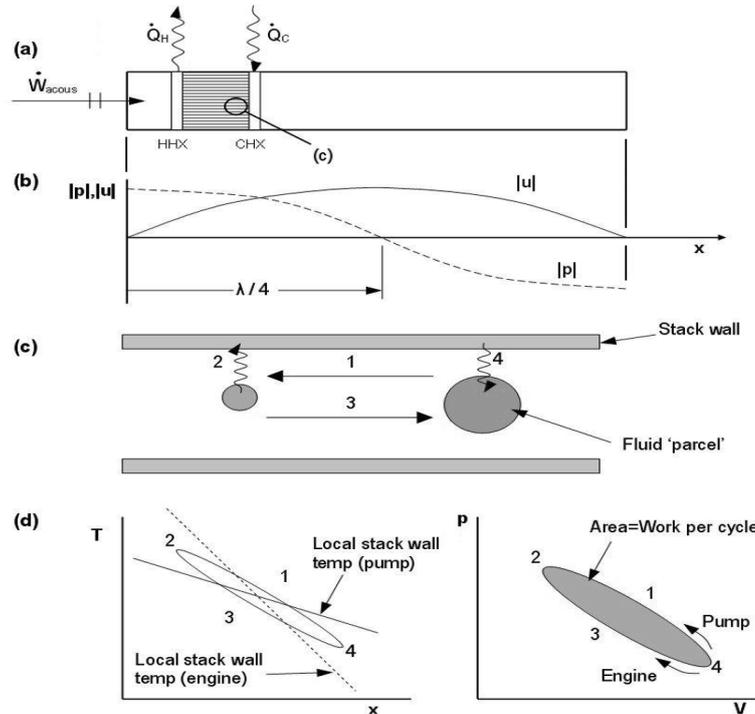


Figure 5. Diagram of automotive thermoacoustic refrigerator(ATAR) system

Standards of Thermoacoustics Figure 6(a) shows a sketch of a basic half-frequency thermoacoustic heat siphon, in which the liquid inside the cylinder is energized by an acoustic source (not shown), like an amplifier or intensity motor. A 'stack' is situated in the cylinder between a hot intensity exchanger (HHX) and a virus heat exchanger (CHX), and its motivation here is to furnish a ceaseless temperature conveyance with purposefully defective warm contact with the swaying liquid. Stacks in thermoacoustic gadgets fluctuate in math and development yet all give a progression of restricted holes through which the liquid wavers. Stacks are

frequently developed from gathering a heap of slender plates (Tijani 2002c), folding up a sheet into a winding (Tijani 2002c) or penetrating openings through a strong billet (Hatazawa 2004). Figure 6(b) shows the dispersion of

Figure 6. Sketch diagram of a half-wavelength thermoacoustic pump; the tube is closed at each end and an acoustic source (such as a loudspeaker) is used to pump heat;(b) Distribution of acoustic pressure and velocity amplitude along the axis of the device shown in (a); (c) Sketch of the thermodynamic cycle of a gas parcel inside the stack shown in (a); (d) Temperature versus position and pressure versus volume for the gas parcel shown in (c). Figure 6(c) shows a close-up



sketch of the stack in Figure 6(a), showing the stages in which the thermoacoustic heat pump cycle operates. The first and second graphs of Figure 6(d) indicate the temperature versus position and pressure versus volume of a parcel of fluid oscillating inside the stack respectively. With reference to Figures 6(c) and 6(d), consider a parcel of fluid oscillating along the axis of the device, in thermal contact with the stack plates. The four stages of the thermoacoustic heat pump cycle the fluid experiences are

1. **Compression:** The parcel of fluid is compressed as it moves from a lower pressure region to a higher pressure region, which causes an increase in its temperature;
2. **Heat Rejection:** The fluid parcel in its compressed state is hotter than the local stack temperature (Figure 6(d)), so heat is transferred to the stack, cooling the parcel of fluid;
3. **Expansion:** The parcel is returned to a lower pressure, and under expansion the fluid experiences a decrease in temperature; and
4. **Heat Withdrawal:** The parcel is now colder than the local stack temperature (Figure 6(d)), so heat is transferred from the stack to the fluid.

Two basic perspectives to the maintainability of the cycle are (a) the warm post-pones related between the stack and the functioning liquid, and (b) the full acoustic climate wherein the cycle happens.

The material of the stack and its encompassing walls for the most part has great warm limit yet unfortunate conductivity, to such an extent that little intensity is led from the HHX to CHX through hub conduction in the wall. It is alluring for the two intensity exchangers to each have great warm conductivity for contact with outside heat sources and sinks. Along these lines, heat is 'siphoned' between the closures of the stack, which are themselves trading heat with the outside of the gadget.

Standing wave thermoacoustic heat motors work backward to warm siphons, with the nearby stack temperature angle higher than that of the cycle, as shown by the ran line in Figure 6(d). A warm slope, dT_m/dx , is made by applying hot or cold temperature sources

to the intensity exchangers. Hypothetically, when the warm angle in the stack surpasses what is generally named the basic temperature slope (∇T_{crit}), an acoustic reaction in the stack is created.

Working Gases

Thermoacoustic frameworks regularly utilize business grade helium, or combinations of honorable gases like helium-argon or helium-xenon. The decision of working gas is frequently founded on the thermoacoustic power thickness, which Quick (2002) demonstrated in a dimensionless examination to be corresponding to pma , the result of the mean strain (pm) and speed of sound of the gas (a). Since helium has the most elevated sound speed and warm conductivity of every single dormant gas (Tijani 2001), it pursues for a superb beginning plan decision. The fast of sound permits the development of moderately high-recurrence gadgets without the vital aspects being excessively little. The high warm conductivity expands the warm entrance profundity of the gadget, which builds the stack calculation to sizes that can be obliged by moderately reasonable assembling strategies (Quick 2002).

Thermoacoustic gadgets are novel among potential auto refrigeration frameworks in their utilization of helium gas. The natural advantages that exist in involving helium in thermoacoustic frameworks over rival advancements incorporate

- zero a worldwide temperature alteration potential (GWP) from direct outflows;
- zero ozone consumption potential from direct emanations;
- the functioning gas doesn't be guaranteed to should be recovered whenever supplanted;
- the functioning gas is non poisonous or combustible; and
- the framework works at similarly lower gas tensions to VC frameworks, decreasing the heaviness of the framework.

Different refrigerants utilized in rival advancements like alkali, butane, propane, HFCs, CFCs, HCFCs, and carbon dioxide have at least one of these issues.

Squander Intensity ENERGY Accessibility

Thermoacoustic refrigeration is a potential option in auto or other vehicle applications since the cycle can be fueled by heat, rather than power or mechanical power. In an auto, the low warm efficiencies of petroleum or even diesel motors bring about a lot of intensity delivered to the climate, through different ways from the place of burning, for example,

- conduction through the ignition chamber walls into the motor cooling framework, leaving by means of the radiator and uncovered pipework;
- conductive exchange from the burning chamber walls to the motor block outside, and afterward convective and radiative exchange to the motor cove compartment;
- heat move from the fumes gas stream to the ventilation system and fumes framework, then, at that point, move to the climate; and
- held heat in the fumes gas stream leaving straightforwardly to the air at the fumes outlet.

Hatazawa et al. (2004), who recommended that as much as 35% of the nuclear power created from burning in an auto petroleum motor was lost to the climate through sweltering fumes gas and other radiation misfortunes. Johnson (2002) showed that for a regular 3.0L petroleum motor with a most extreme result force of 115kW, the all out squander heat scattered can differ from 20kW to as much as 400kW across the scope of normal motor activity.

Horuz (1999) drove a homegrown smelling salts water VAR arrangement (of 10kW evaluated limit) utilizing the fumes gas stream of a 6-liter turbocharged diesel motor, as utilized in enormous street transport vehicles. Horuz (1999) determined the expected intensity contribution to arrive at full ability to be 23.2kW, a warming burden he exhibited to exist in the fumes gas stream for motor results above 35kW and 200Nm. Garrabrant (2003) assessed the normal accessible intensity energy in the fumes stream of a commonplace truck diesel motor, (for example, that utilized by Horuz) at full motor burden to be 66kW, though Horuz assessed it to be 120kW (with a motor result of ~103kW and ~470Nm) (Horuz 1999). Anyway both Horuz and Garrabrant recognize that adequate ability to work a VAR framework is unavailable during inactive circumstances and low choke inputs.

For a regular driving cycle, the time-found the middle value of accessible warming power is around one to two significant degrees over the expected cooling power. Johnson (2002) noticed that for a run of the mill and delegate driving pattern of a three-liter petroleum motor, the normal warming power accessible was

~23kW, contrasted with the 0.8 with 3.9kW of cooling limit given by normal traveler vehicle VC frameworks (Gschneidner

2002, Bhatti 1999a, 1999b). Besides, in the occasion of a transport forced air system, refrigerant blowers are in many cases driven by a different more modest motor. In the event that a thermoacoustic fridge with adequate cooling limit could be driven utilizing the intensity from the diesel motor's fumes gas just, the blower and its related more modest motor could be disposed of by and large.

Hatazawa et al. (2004) utilized heat from the fumes gas of a 4-stroke car petroleum motor to drive a standing wave heat motor. The driving force of Hatazawa et al. utilized almost no intensity input, was not tightened to address Rayleigh streaming, and was of little breadth (30mm) and limit ($W_{acous}=3W$) (M Hatazawa 2004, pers. comm., 30 September), but their examination affirmed that at normal working paces, adequate temperatures and promising degrees of warming power were available in the fumes gas. For stable activity, warm contributions to the thermoacoustic motor of Hatazawa et al. were accounted for to be in overabundance of 300W and at over 300°C, accomplished with a motor speed of 2600rpm and a choke opening of 35% (M Hatazawa 2004, pers. comm., 30 September).

Notwithstanding, how much intensity energy in a fumes gas stream could be expanded by diminishing the intensity move into the motor block, which thus could prompt an expanded acoustic power yield. Research by Taymaz et al. (2003) showed that heat misfortunes into the motor block of a diesel motor could be decreased as much as 25% by covering the inside essences of the chamber and cylinder with a 0.5mm thick composite earthenware layer. Utilization of the insulative layer was displayed to additional increment the nuclear power and in this manner the temperature of the fumes gas. This would likewise expand the ignition proficiency of the motor.

Wendland (1993) determined that at low Reynolds numbers (low motor rates), almost 50% of the all out heat misfortune in an ordinary standard fumes framework happened in the motor complex segment. It would be sensible to expect that for consistent activity while the motor is out of gear, a reasonably planned thermoacoustic fridge would be situated in the close to area to the ventilation system or quickly downstream of the exhaust system, or an electric warming loop would be utilized to expand the accessible fumes gas warming power.

PRELIMINARY DESIGN OF A HEAT-DRIVEN THERMOACOUSTIC REFRIGERATOR

A reasonable plan of an intensity driven thermoacoustic fridge (HDTAR) is displayed in Figure 7. This plan is like the 'lager cooler' depicted by Wheatley et al. (1986) in that the thermoacoustic motor is set near the intensity siphon, with the encompassing intensity exchanger (AHX) of each nearest together. Along these lines, the four intensity exchangers are situated arranged by dropping working temperature from hot (HHX) to encompassing (AHX1 and AHX2) to cold (CHX). Wheatley et al. (1986) recognize this plan of thermoacoustic motor and siphon is poor. The intensity siphon, which involves a clay substrate stack sandwiched between the second encompassing intensity exchanger (AHX2) and cold intensity exchanger (CHX), ought to in a perfect world be found nearer to the shut (left as displayed) end, where the strain sufficiency is boosted and acoustic speed (and related gooey misfortunes) is at any rate. The HDTAR is roughly 950mm long, with clay stacks 50mm in ostensible distance across.

To lessen development costs, the HDTAR is planned utilizing large numbers of the parts utilized for the amplifier driven thermoacoustic fridge (TAR) that was finished in late 2004. The HDTAR is intended for use with helium

compressed to 700kPa, according to the current 2003 TAR plan. This was to limit producing costs thus that examinations in the working qualities between utilizing the thermoacoustic heat motor and the amplifier could be made.

The displaying program DeltaE (Ward and Quick 2003) is a valuable plan device in the improvement of thermoacoustic frameworks. By entering the calculation and materials utilized in the development of the HDTAR into DeltaE, the cooling execution of the gadget can be assessed for different working circumstances. For the primer plan of the HDTAR, an intensity contribution of $Q_{exh,H}=300W$ and an ideal cooling force of $Q_{int,C}=30W$ with a surrounding temperature of 27°C were inconsistent picked. For these circumstances, DeltaE assessed the crucial reverberation recurrence to be 256Hz. For this recurrence of activity, DeltaE was utilized

to decide the consistent state temperature contrast accomplished at the CHX. In a car application, the CHX would hypothetically be in touch with return air to the vehicle inside.

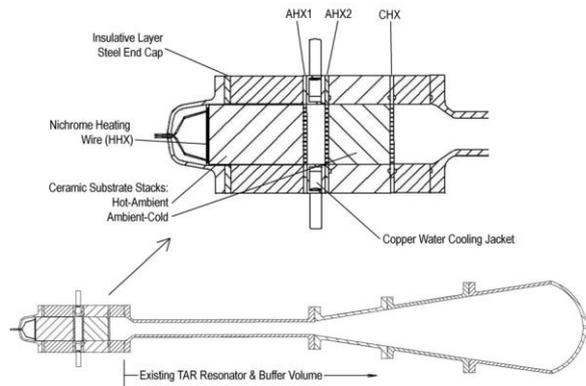


Figure 7. Cross sectional view of conceptual heat-driven 2003 TAR (HDTAR).

Figure 8 shows predictions made with DeltaE of several key parameters of the system under steady state operation. The internal axial coordinate x , where $x=0$ is on the left side of the HDTAR shown in Figure 7. As one would expect, particle velocities at each rigid end of the device are zero, and a pressure node (velocity antinode) exists at the end of the resonator. Also notable is the generation (increase) of acoustic power in the heat engine (HHX to AHX1) which is consumed in the heat pump (AHX2 to CHX).

As shown in Figure 8, DeltaE estimated the CHX and resonator temperature to be $\sim 2^\circ\text{C}$, for 30W of cooling capacity and a 300W heat input. The maximum acoustic pressure amplitude was estimated to be $\sim 186\text{kPa}$ (199dB re $20\mu\text{Pa}$) at $x=0$, and the maximum acoustic particle velocity to be 252ms^{-1} (Mach ~ 0.25) at the resonator termination ($x=0.64\text{m}$).

Practical Considerations for an Automotive Thermoacoustic Refrigerator (ATAR)

The cooling limit of the ATAR could be expanded by combining numerous ATAR units. The power thickness could be expanded by expanding the mean strain of the functioning liquid from 700kPa to say 1.5MPa.

The size of the ATAR could be decreased by winding the resonator into helix or twisting. In a creation variant, high strength infusion formed plastics, for example, ABS could be utilized to accomplish this shape, give a smooth interior completion and limit weight. In the event that the uncoiled length of the gadget was 500mm, the working recurrence would be around 1,000Hz assuming helium gas was utilized as the functioning liquid.

A significant degree gauge for the complete pace of intensity traded at each intensity exchanger (H2) (for example absolute force) of the proposed ATAR was determined utilizing Quick (2002, Eq. 5.33):

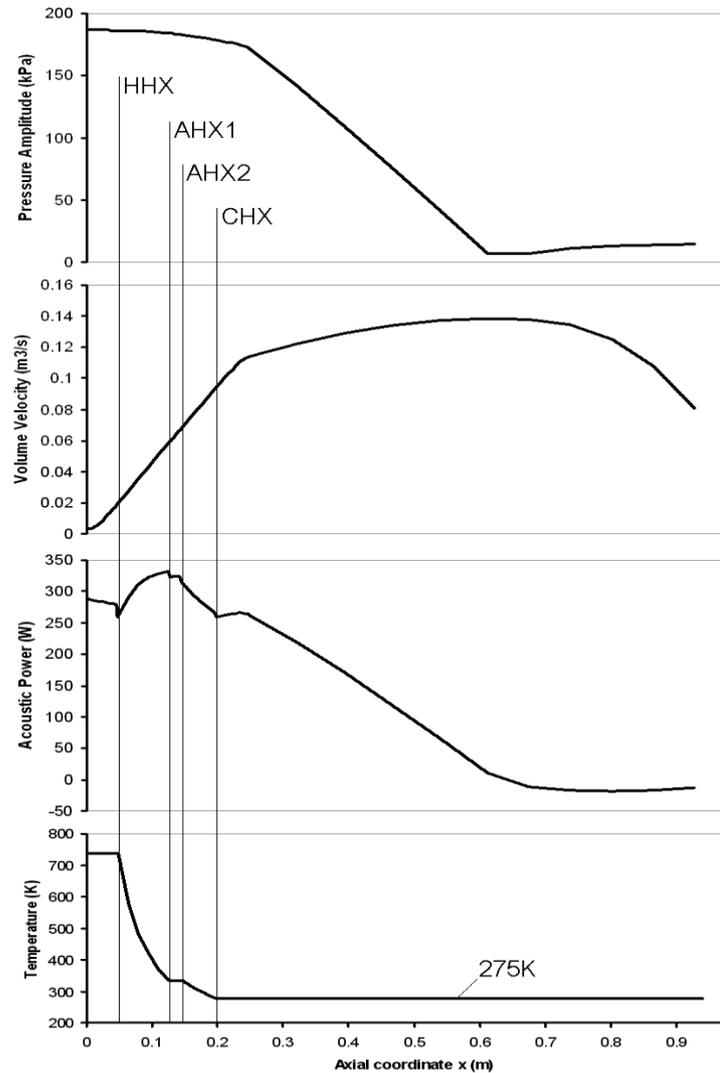


Figure 8. State variable plot of the HDTAR using 700kPa helium, 300W heat input, 30W cooling load, 256Hz operating frequency.

DISCUSSION

The costs in executing a creation prepared thermoacoustic framework in a car application appear to unequivocally offset those of VC frameworks and option car refrigeration frameworks examined here. The two biggest worries with such an application, being cooling limit and accessible warming power, are not impossible obstructions to the improvement of the innovation as a substitution. Progresses in the plan and comprehension of high-sufficiency thermoacoustic frameworks will prompt more productive, strong frameworks, and the utilization of electrical radiator components to expand the fumes gas warming power is a potential choice.

CONCLUSION

Of all the alternative refrigeration technologies considered as replacements for automotive vapour-compression systems, thermoacoustic refrigeration is most appealing in terms of economic and environmental benefits.

Practical considerations and performance estimates indicate that an automotive waste-heat driven thermoacoustic air-conditioner is functionally feasible, however further investigation is needed with regards to sufficient cooling capacity.

ACKNOWLEDGEMENTS

The authors would like to thank the Mazda Foundation for their generous support. The authors would also like to thank the

administrative, technical and workshop staff at the School of Mechanical Engineering, University of Adelaide, for their assistance in many aspects regarding this work.

REFERENCES

- Backhaus, S.N., and Swift, G.W. (2002) 'New varieties of thermoacoustic engines', *Proceedings of the Ninth International Congress on Sound and Vibration*, Orlando FL, July 8-11, vol. 502.
- Bansal, P.K., and Martin, A. (2000) 'Comparative study of vapour compression, thermoelectric and absorption refrigerators', *Int. J. Energy. Res.*, vol. 24, pp. 93–107.
- Bhatti, M.S. (1999a) 'Enhancement of R-134a automotive airconditioning system', *SAE Technical Paper*, no. 1999-01-0870.
- Bhatti, M.S. (1999b) 'Evolution of automotive airconditioning - riding in comfort: Part II', *ASHRAE Journal*, September.
- Brown, J.S., Yana-Motta, S.F. and Domanski, P.A. (2002) 'Comparative analysis of an automotive air conditioning systems operating with CO₂ and R-134a', *Int. Journal of Refrigeration*, vol. 25, pp. 19–32.
- Butler, D. (2001) *Life after CFCs and HCFCs*. Technical report, Building Research Establishment (BRE), Watford UK.
- DiSalvo, F.J. (1999) 'Thermoelectric cooling and power generation', *Science*, vol. 285, pp.705–706.
- Garrabrant, M.A. (2003) 'Proof-of-concept design and experimental validation of a waste heat driven absorption transport refrigerator', *ASHRAE Transactions*, vol. 109 no. 1, pp. 401–411.
- Gentner, H. (1998) 'Passenger car air conditioning using carbon dioxide as refrigerant', *Proceedings of the Natural Working Fluids '98*, IIR-Gustav Lorentzen Conference, Oslo, Norway, pp. 303–313.
- Gschneidner, K.A., Pecharsky, V.K., Jiles, D. and Zimm, C.B. (2002) *Development of vehicle magnetic air conditioner technology*. Technical report, Institute for Physical Research and Technology, Iowa State University, Iowa.
- Hatazawa, M., Sugita, H., Ogawa, T. and Seo, Y. (2004) Performance of a thermoacoustic sound wave generator driven with waste heat of automobile gasoline engine. *Transactions of the Japan Society of Mechanical Engineers (Part B)*, vol. 70, no. 689, pp. 292–299.
- Horuz, I. (1999) 'Vapor absorption refrigeration in road transport vehicles', *Journal of Energy Engineering*, vol. 125, no. 2, pp. 48–58.
- Ioffe, A.F. (1957) *Semiconductor thermoelements and thermoelectric cooling*. Infosearch, London.
- Johnson, V.H. (2002) Heat-generated cooling opportunities in vehicles', *SAE Technical Papers*, no. 2002-01-1969.
- Lang, R., Roth, M., Stricker, M. and Westerfield, T. (1999) 'Development of a modular zeolite water heat pump', *Heat and Mass Transfer*, vol. 35, pp. 229–234.
- Leivo, M.M., Pekola, J.P. and Averin, D.V. (1996) 'Efficient Peltier refrigeration by a pair of normal metal / insulator /superconductor junctions', *Appl. Phys. Lett.*, vol. 68, no. 14, pp. 1996–1998.
- Lu, Y.Z., Wang, R.Z., Jianzhou, S., Zhang, M., Xu, Y.X. and Wu, J.Y. (2003) *Performance of a diesel locomotive waste-heat-powered adsorption air conditioning system*. Technical report, Inst. of Refrigeration and Cryogenics, Shanghai Jiao Tong University, Shanghai 200030, China.
- Mei, V. (1979) 'A truck exhaust gas operated absorptionrefrigeration system', *ASHRAE Transactions*, vol. 85, pp.66–76.
- Moran, M.J. and Shapiro, H.N. (2000) *Fundamentals of Engineering Thermodynamics*. John Wiley and Sons Inc, New York.
- Peltier, J.C. (1834) 'Nouvelles experiences sur la caloricité des courans electriques', *Annales de Chimie*, vol. 56, pp. 371–387.
- Seebeck, T.J. (1822) 'Magnetische polarisation der metalle und erze durch temperatur-differenz', *Abhandlugen der Deutschen Akademie der Wissenschaften zu (Berlin)*, pp. 265–373.
- Sun, D., Qiu, L., Zhang, W., Yan, W. and Chen, G. (2004) 'Investigation on travelling wave thermoacoustic heat engine with high pressure amplitude', *Energy Conversion and Management*, vol. 46, pp. 281–291.
- Swift, G.W. (2002) *Thermoacoustics: A unifying perspective for some engines and refrigerators*. Acoustical Society of America, Melville, NY.
- Taymaz, I., Cakir, K., Gur, M. and Mimaroglu, A. (2003) 'Experimental investigation of heat losses in a ceramic coated diesel engine', *Surface and Coatings Technology*, vol. 169-170, pp. 168–170.